



GEOTECHNICAL INVESTIGATION REPORT

PROPOSED SENIORS LIVING DEVELOPMENT
671 - 683 OLD SOUTH HEAD ROAD, VAUCLUSE NSW

PREPARED FOR
OSHR AT VAUCLUSE HOLDINGS PTY LTD
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1 PROJECT INFORMATION

1.1 INTRODUCTION AND OBJECTIVE

Geo-Environmental Engineering Pty Ltd (GEE) was commissioned by Blare Management, on behalf of OSHR At Vaucluse Holdings Pty Ltd, to complete a geotechnical investigation at 671 - 683 Old South Head Road, Vaucluse New South Wales (herein referred to as the 'site') which relates to the proposed construction of a multi-storey seniors living development with a two-level basement. An in-ground swimming pool is also proposed at the rear of the site.

A survey plan showing existing site features is provided in **Appendix A**. The site covers an approximate area of 3,908.08m² (by calculation) and encompasses the following legal allotments:

- ◊ Lot B in Deposited Plan (DP) 324744
- ◊ Lot 2 in DP 10314
- ◊ Lot 1 in DP 169310
- ◊ Lot 4 in DP 192614
- ◊ Lot 1 in DP 168877
- ◊ Lot 1 in DP 167942
- ◊ Lot 1 in DP 666626
- ◊ Lot 2 in DP 316716

The investigation was required to support a Development Application with Waverley Council and to assist with the preliminary design of the development. The investigation also complements a previous geotechnical investigation and report completed by Crozier Geotechnical Consultants in 2018 (reference 2) for part of the site (i.e. 671 – 679 Old South Head Road).

The report presents the factual results of the field investigations and provides interpretation and recommendations regarding the ground conditions at the site in accordance with client requirements and the agreed scope of work.



1.2 PROPOSED DEVELOPMENT

The proposed development comprises the demolition of an existing low-density residential properties and the construction of a multi-storey seniors living development with a two level basement for parking and general storage.

According to the architectural plans, a copy of which is provided in **Appendix A**, the lowest basement level will have Finished Floor Level of 61.5m above Australian Height Datum (AHD) and vehicle access will be possible from Old South Head Road via a ramp at the northern end of the development. The access ramp to the basement will extend up to the northern boundary while the remainder of the basement levels will be setback at least 2.2m from the boundaries. Considering the existing surface levels as shown on the survey plan, and the necessary over excavation to accommodate the basement floor slab, GEE anticipates an excavation depth of between approximately 5.0m and 12.0m. The deepest excavation will occur at the southern end of the site.

The depth of the proposed pool is not known although GEE expects it to require excavation to a depth of between 1.0m and 2.0m with this excavation setback approximately 2.0m from the boundaries.

1.3 PREVIOUS INVESTIGATION

As previously mentioned, Crozier Geotechnical Consultant completed a geotechnical investigation across part of the site (i.e. 671 – 679 Old South Head Road) in 2018 (reference 1) which included:

- ◊ The drilling of five auger boreholes along with the performance of Dynamic Penetrometer (DCP) testing to investigate the subsurface geology, depth to bedrock and identification of ground water conditions, and
- ◊ Detailed geotechnical mapping of the site and adjacent properties including photographic record of site conditions by an experienced Geotechnical Engineer.

A copy of the borehole logs and DCP test data is provided in **Appendix B**. A site plan showing the location of their boreholes and DCP tests is provided as **Figure 1**.

1.4 SCOPE OF WORK

The scope of work undertaken by GEE, to satisfy the above objective, was as follows:

- ◊ Visual appraisal of the site conditions and locality,



- ◊ Review of a previous geotechnical report completed for the adjoining residential development at 671 – 679 Old South Head Road (reference 1),
- ◊ Review of geological, soils and acid sulfate soil maps relevant for the site,
- ◊ The drilling and logging of two additional boreholes (BH201 and BH202) to compliment the previous boreholes drilled by Crozier Geotechnical Consultants in 2018,
- ◊ The performance of Standard Penetration Tests and a Dynamic Cone Penetrometer (DCP) test to assess the consistency and/or relative density of the soil profile,
- ◊ The collection of representative soil samples for the preliminary assessment of soil salinity and aggressivity, and
- ◊ Engineering assessment and reporting.



2 SITE INFORMATION

2.1 SITE DESCRIPTION

The site is an irregular parcel of land situated on the eastern corner of Old South Head Road.

At the time of this investigation the site comprised seven residential properties, each containing a house with associated gardens/access pathways, sheds/outbuildings, paved areas and scattered trees. Photographs of the frontages of each property are provided below as **Plates 1 to 7**.

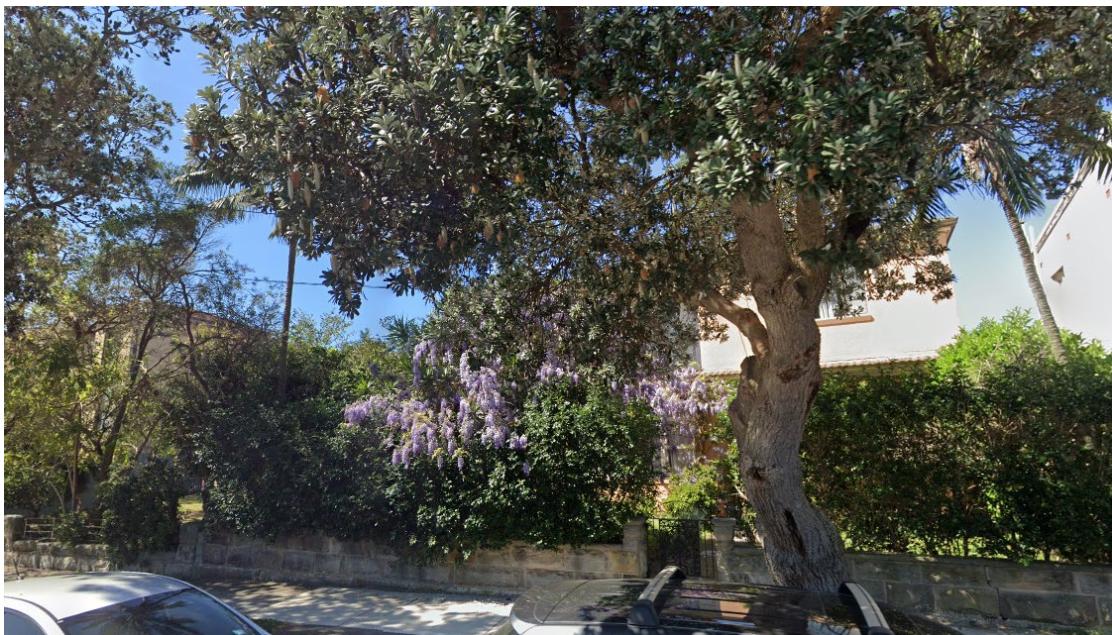


Plate 1: Front of No. 671 Old South Head Road (Source: Google Street View)

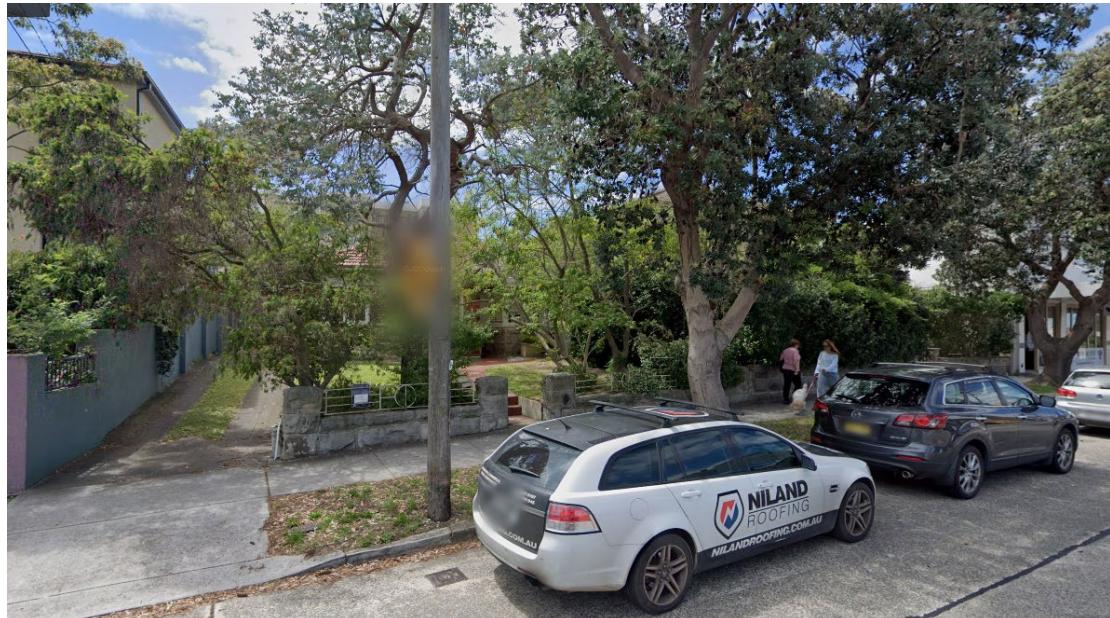


Plate 2: Front of No. 673 Old South Head Road (Source: Google Street View)

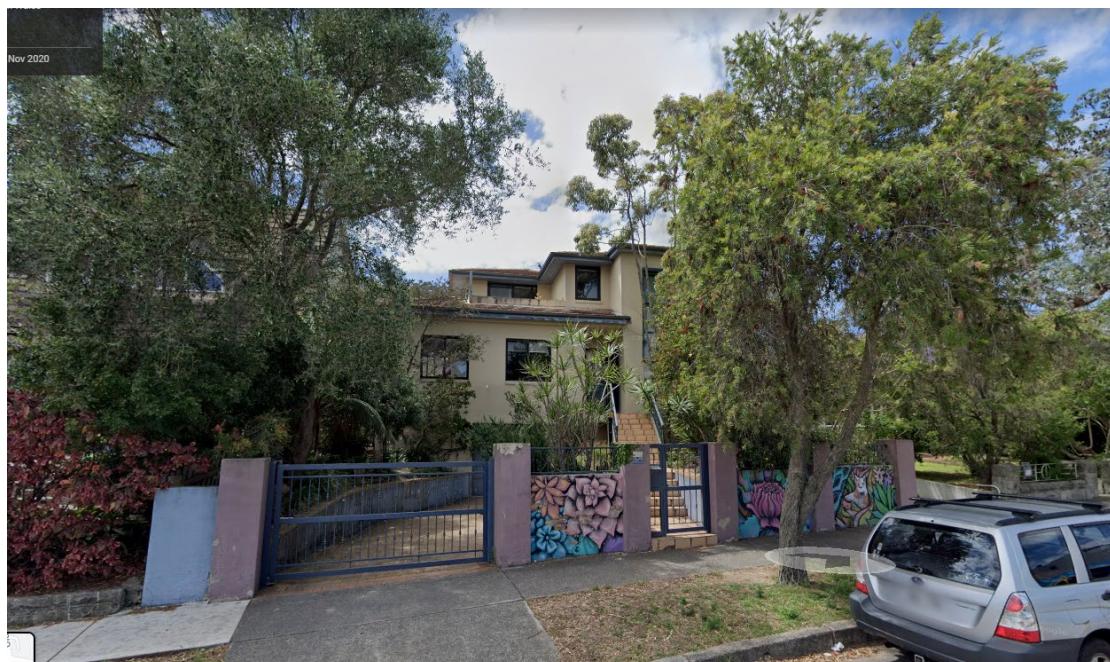


Plate 3: Front of No. 675 Old South Head Road (Source: Google Street View)

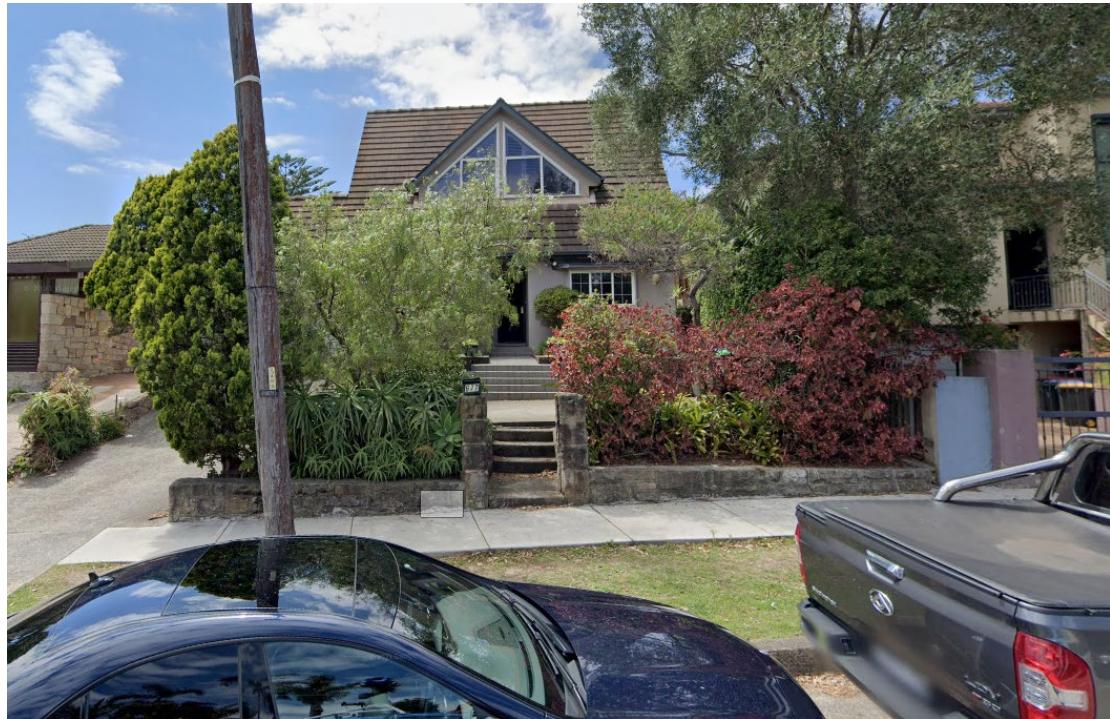


Plate 4: Front of No. 677 Old South Head Road (Source: Google Street View)



Plate 5: Front of No. 679 Old South Head Road (Source: Google Street View)



Plate 6: Front of No. 681 Old South Head Road (Source: Google Street View)

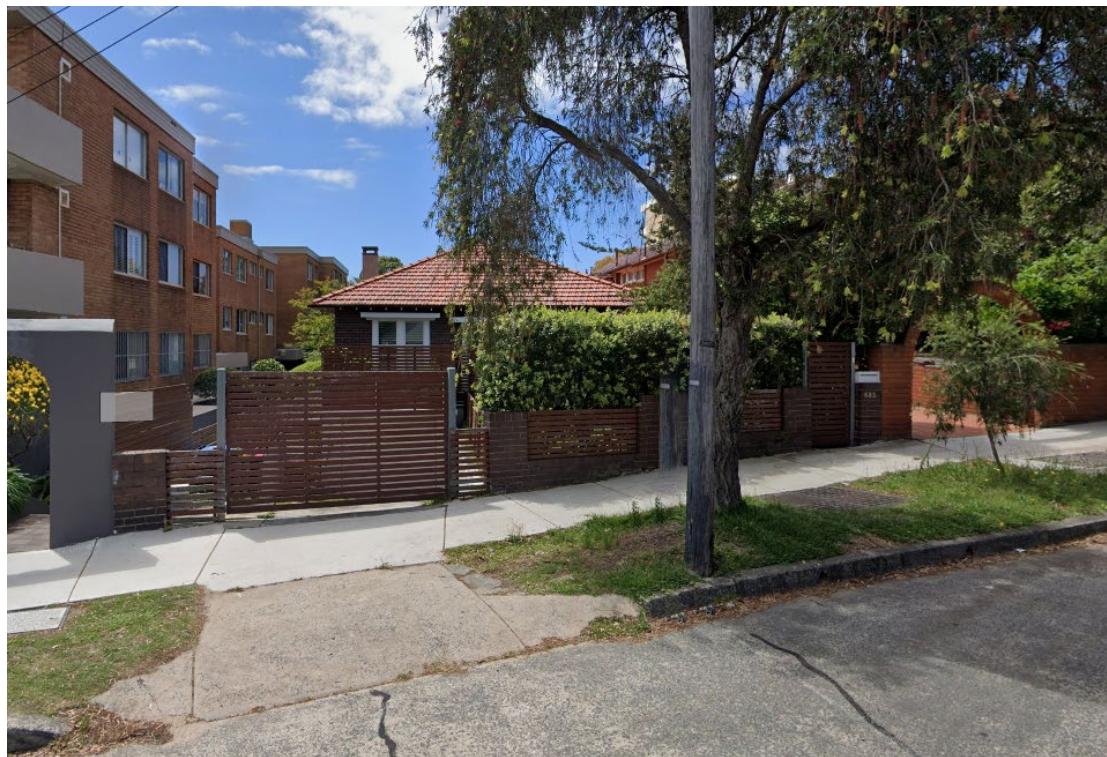


Plate 7: Front of No. 683 Old South Head Road (Source: Google Street View)



2.2 TOPOGRAPHY

The site is located about mid-way on a gentle to moderately north dipping slope. The surface elevation as shown on the survey plans (**Appendix A**) vary between approximately 73m AHD at the southern boundary and 66m AHD at the northern boundary.

2.3 GEOLOGY AND SOILS

2.3.1 Regional

A review of the regional geological map (reference 2) indicates that the site is underlain by the Hawkesbury Sandstone formation, which typically consists of "...medium to coarse-grained quartz sandstone, very minor shale and laminitic lenses". The map also indicates that the site is within close proximity (~200m) to the Quaternary aged Alluvium formation which comprises "...medium to fine-grained 'marine' sand with podsols".

A review of the regional soils map indicates that the site is located within the Lambert Soil Landscape Group (reference 3) which is associated with undulating to rolling rises and low hills on Hawkesbury Sandstone. Local reliefs are up typically 20-120m and slopes are usually less than <20% in gradient, with frequent rock outcrops (>50%). Soils of the Lambert Group typically comprise erosional sands and clays, have seasonally perched water tables and very low soil fertility.

2.3.2 Site Specific

A broad summary of the subsurface conditions observed in the previous investigation by Crozier Geotechnical Consultants (reference 1) is provided below:

- "**TOPSOIL/FILL** – this layer was encountered at all test locations to a maximum depth of 0.95m (BH4) and comprised fine to medium grained sand.
- **SAND (Superficial Soils)** – this deposit was encountered at all test locations to the maximum depth of investigation of 5.80m (BH5) with the exception of BH1 where the base of the deposit was encountered at a depth of 2.60m. The deposit comprised fine to medium grained, poorly graded sand which varied in density between very loose to very dense and is considered to represent Quaternary 'dune' sand. Podsol horizons (bleached sand over cemented sand) were encountered within this soil at several locations/levels.
- **Gravelly SAND (Superficial Soils)** – This layer was only encountered within BH1 between 2.60 and 2.80m depth. The deposit comprised medium dense, fine to



medium grained sand with sub-rounded gravel and is a characteristic deposit found at the base of the Quaternary sands.

- **Sandy CLAY (Residual soils)** – Firm clay which rapidly became very stiff to hard was only encountered within BH1 underlying the gravelly sand and represents a residual soil derived from the weathering of the underlying Hawkesbury Sandstone.
- **SANDSTONE (Bedrock)** – What has been interpreted extremely low strength sandstone bedrock was only encountered in BH1 below approximately 3.60m however the distinction between residual soils and bedrock should be considered approximate and gradational.”

2.4 HYDROGEOLOGY

2.4.1 Regional

The regional and permanent groundwater in the vicinity of the site, is expected to be confined or partly confined, discrete, water-bearing zones within the bedrock formation, or partly confined, perched water tables within the sand profile. Intermittent water flow or seepages are likely to occur through defects in the exposed sandstone outcrop, on the sand-residual soil interfaces or residual soil-rock interfaces, especially during periods of heavy rainfall.

2.4.2 Site Specific

Permanent groundwater (i.e. the water table) was not identified in the previous boreholes drilled by Crozier Geotechnical Consultants.

2.5 ACID SULFATE SOIL RISK

Acid sulfate soils are naturally occurring sediments and soils containing iron sulfides (principally iron sulfide, iron disulfide or their precursors). Oxidation of these soils through exposure to the atmosphere or through lowering of groundwater levels results in the generation of sulfuric acid.

Land that may contain potential acid sulfate soils was mapped by the NSW Department of Land and Water Conservation (DLWC) and based on these maps local Councils produced their own acid sulfate soil maps to be used for planning purposes.

The DLWC 'Sydney Heads' Acid Sulfate Soil Risk Map (reference 4), indicates that the site lies within an area with no known occurrences of acid sulphate soil and land activities within this area are "...not likely to be affected by acid sulphate soil materials".



The Acid Sulfate Soils Map produced by the NSW Department of Planning and Environment, via interactive online mapping, indicates that the site lies outside of areas defined as '*Class 1*' to '*Class 5*'. In this regard, there is no need for an acid sulphate soil assessment or management plan.



3 METHOD OF INVESTIGATION

Fieldwork was completed in by Stephen McCormack from GEE on the 19th August 2021 and comprised the following activities:

- ◊ The drilling and logging of two boreholes (BH201 and BH202) to better assess the subsurface conditions across the site,
- ◊ The performance of SPT and DCP tests at the borehole locations to assess the consistency and/or relative density of the soil profile, and
- ◊ The collection of representative soil samples for the preliminary assessment of soil salinity and aggressivity.

3.1 BOREHOLE DRILLING AND SPT/DCP TESTING

Prior to commencement of the bores, an inspection for potential underground services and utilities was completed and cross-checked with the results of a Dial Before you Dig (DBYD) search.

Borehole BH201 was drilled at the front of No. 683 Old South Head Road, which is also the north-western corner of the site, using a truck mounted drilling rig that was owned and operated by the FICO Group, utilising solid flight augers (SFA). SPTs were performed in borehole BH201 in accordance with Australian Standard (AS) 1289.6.3.1 (reference 5).

Borehole BH202 was drilled at the rear of No. 683 (north-eastern corner of the site) using an 85mm diameter, hand operated, auger, while the DCP tests were performed in accordance with Australian Standard test method AS1289.6.3.2-1997 (reference 6).

During the drilling of each borehole the encountered fill and natural soils were geologically logged taking care to describe the presence and depth of fill material / previously disturbed ground, the natural stratum, moisture, seepages or water bearing zones. At the completion of each borehole, they were backfilled with soil cuttings and the surface reinstated. Both boreholes were advanced through a surface layer of topsoil and the underlying natural sand soil profile before terminating within the underlying sandstone bedrock formation at a depth of 2.2m bgs at BH201 and 3.95m bgs at BH202.

The location of the boreholes and DCP tests was estimated using measurements from existing features and is shown on **Figure 1**. A copy of the borehole log (including SPT and DCP test data) is provided in **Appendix B**.



3.2 SOIL SAMPLING

Soil samples were collected at regular intervals from each of the boreholes and selected samples were submitted to Eurofins laboratory for the following NATA accredited testing as part of a preliminary assessment of soil salinity and soil aggressivity towards buried concrete and/or unprotected steel.



4 INVESTIGATION RESULTS

4.1 SUBSURFACE CONDITIONS

The site stratigraphy, as observed in the previous boreholes and the recent boreholes drilled by GEE typically comprised a layer of topsoil and/or fill material overlying natural sand which was underlain by sandstone bedrock which is consistent with the Hawkesbury Sandstone formation.

Detailed descriptions of the subsurface conditions on site are provided in the borehole logs provided in **Appendix B**, while the generalised soil profile is provided in **Table 1**. Two geological sections (A-A' and B-B') are also provided in **Figure 2**.

Table 1: Summary of Subsurface Conditions – Geological Model

Layer / Unit	Description	Depth to the Top of Layer (m)	Consistency / Relative Density ⁽¹⁾
1 - TOPSOIL / FILL	SAND: dark brown and grey, fine to medium grained with trace roots and silt.	0.0	Very loose to loose
2a - NATURAL SOIL	SAND: grey, brown, orange-brown, fine to medium grained with a band of partially indurated nodules.	0.2 – 0.95	Loose
2b - NATURAL SOIL		1.0 – 2.3	Medium Dense (or better)
3 - BEDROCK	SANDSTONE: grey and orange, weathered.	2.0 to >5.8m	--

4.1.1 *Groundwater*

Permanent groundwater (i.e. the water table) was not encountered during the drilling of the boreholes and is expected to be present within the bedrock formation. However, perched seepage water was observed near the interface of the residual soil and bedrock formations. This water is directly recharged by rainfall events and therefore its presence and volume will vary significantly.



4.2 LABORATORY TEST RESULTS

Representative samples of soil were collected from each borehole and submitted to Eurofins MGT laboratory for selective testing which included:

- ◊ Electrical Conductivity (EC) to provide a detailed assessment of the salinity potential of the soil profile, and
- ◊ Sulphate, Chloride, resistivity and pH to determine the exposure classification of the soil with respect to buried structural concrete and unprotected steel.

The laboratory test results are presented in **Appendix C**, while a summary of the results is provided in the following sub-sections.

4.2.1 Soil Salinity Testing

An assessment of soil salinity conditions has been undertaken with reference to guidance published by the Department Land and Water Conservation NSW (reference 7). In this regard, selected samples of natural soil were submitted to Envirolab for NATA accredited testing of Electrical Conductivity (EC), which is the primary indicator of salinity,

The raw EC results and the EC_e results¹, are provided in **Table 2**.

Table 2: Electrical Conductivity Results

Sample Location / Depth	Sample Description	EC (dS/m)	Multiplication Factor ¹	EC _e (dS/m)
BH201/1.0 – 1.45m	SAND	0.018	17	0.31
BH201/1.6 – 1.8m	SAND	0.016	17	0.27
BH202/1.2 – 1.5m	SAND	0.016	17	0.27
BH202/2.3 – 2.5m	SAND	0.022	17	0.37
BH202/3.3 – 3.5m	SAND	0.010	17	0.17

According to the Department Land and Water Conservation NSW (reference 9) the soil salinity classes are as follows:

¹ EC_e results are EC data multiplied by a conversion factor which depends upon the soil texture / type (Reference 6)



<u>ECe (dS/m)</u>	<u>Class</u>
<2	Non Saline
2 – 4	Slightly Saline
4 – 8	Moderately Saline
8 – 16	Very Saline
>16	Highly Saline

The above test data indicate that the fill/natural soil profile is non-saline.

4.2.2 *Aggressivity Testing*

A limited number of soil samples were analysed for pH, sulfate, chloride and resistivity to provide a preliminary assessment of the exposure classification (or aggressiveness/corrosiveness potential) of the soil with respect to future buried steel and/or concrete (e.g. footings).

To determine the aggressiveness of the soil and water environment on concrete or steel, the chemical test results are compared to Table 6.4.2(C) and Table 6.5.2(C) from Section 6 of the Australian Standard AS 2159 (reference 8). This section provides assessment criteria to assess the 'exposure classification' for a concrete or steel pile. The Standard has two classes of soil conditions:

- (A) high permeability soils below groundwater; and
- (B) low permeability soils and all soils above groundwater.

For this site, the soil samples are considered to be condition 'B' and based on the chemical testing results, the standard provides a range of 'exposure classifications' from non-aggressive to very severe. For the range of chemical conditions in the soil surrounding the structure, the condition leading to the most severe aggressive conditions is adopted.

A summary of the soil results is provided in **Table 3**.



Table 3: Exposure classification (aggressivity) test results

Location / Depth (m bgs)	Soil Condition	pH	Sulphate (SO₄) mg/kg	Chloride (Cl) mg/kg	Resistivity Ohm.cm
BH201/1.0 – 1.45m	B	7.0	<10	<10	54.000
BH201/1.6 – 1.8m	B	6.9	<10	<10	62.000
BH202/1.2 – 1.5m	B	6.3	<10	<10	62.000
BH202/2.3 – 2.5m	B	6.2	13	10	45.000
BH202/3.3 – 3.5m	B	6.6	<10	<10	97.000

The aggressivity potential of an environment on concrete is dependent on the sulphate and pH levels of the soil. Based on the limited number of test results above and taking into account the 'worst-case' sample, the subsurface profile is non-aggressive towards concrete. According to Australian Standard AS 3600-2009 (reference 9), specifically Table 4.8.1, this equates to an exposure classification of 'A1'.

The corrosive potential of an environment on unprotected steel is normally dependent on pH, chloride, and resistivity levels of the soil. Based on the limited number of test results above and taking into account the 'worst-case' sample, the subsurface profile is considered to be non-aggressive towards any unprotected steel.



5 DISCUSSION

5.1 SITE PREPARATION

Following demolition of the existing structures and prior to bulk excavation works, all topsoil with organic matter and any pavement materials, should be removed from the proposed building and pavement areas. Stripped topsoil should be stockpiled for re-use as landscape material or disposed off-site.

Material removed from site will need to be managed in accordance with the provisions of current legislation and may include segregation by material type classification in accordance with NSW EPA (2014) Waste Classification Guidelines (reference 10) and disposal at facilities appropriately licensed to receive the particular materials. GEE notes that the natural soil and bedrock may be classified as Virgin Excavated Natural Material (VENM) and re-used on other sites rather than disposed at a landfill, although it must be proven to be free of contamination.

Also, considering the proximity of adjoining buildings, care must be taken during demolition works to ensure that the adjoining footings, or the zone of influence of these footings, are not disturbed.

5.2 EARTHWORKS

Earthworks at the site is expected to require comprise excavation to a depth of between approximately 5.0m and 12.0m to construct the proposed basement. The access ramp to the basement will extend up to the northern boundary while the remainder of the basement levels will be setback at least 2.2m from the boundaries.

Elsewhere, excavation to a depth of between 1.0m and 2.0m will be required for the proposed pool at the rear of the site with this excavation setback approximately 2.0m from the boundaries.

5.2.1 *Expected Excavation Conditions*

Based on our geological sections A-A' and B-B' (**Figure 2**), the proposed basement excavation will encounter predominately sandy soil and then sandstone bedrock. The pool excavation is expected to be wholly within the sandy soil profile, although this should be confirmed prior to installation.

GEE notes that the strength of the bedrock has not been assessed as part of this geotechnical investigation, however, based on local knowledge, it is likely to be initially



very low to low strength becoming medium to high strength soon thereafter. To confirm the strength of the bedrock within the depth of proposed excavation, a more detailed investigation would be required (preferably following demolition of the existing dwelling) and would need to include the coring and strength testing of the bedrock formation.

The excavation of the soil profile is expected to be readily excavated using standard equipment such as excavators. However, the use of an impact hammer is likely to be required upon encountering the bedrock formation, especially when combined with unfavourable rock-defect geometry. When using an impact hammer the effects of vibration should be considered and are discussed further in Section 5.2.4.

5.2.2 *Groundwater Inflow / Seepage Water*

Permanent groundwater was not encountered during the drilling of the boreholes and will not be encountered by the proposed earthworks. However, water seepages are likely to occur on the contact between soil and bedrock and from defects within the underlying sandstone formation. Such seepages are directly recharged by rainfall and therefore will be intermittent and vary significantly.

The flow of seepage water is expected to be sufficiently managed during the earthworks phase by pumping from a sump at the base of the excavation. In the long term, GEE recommends that the subsurface walls be watertight and conventional techniques such as strip drains, and ag lines will need to be incorporated into the design of these walls to ensure that the flow is not impeded.

5.2.3 *Excavation Support*

Temporary batters are not recommended for proposed basement and pool excavations. Rather, temporary and permanent support (as part of the final basement structure) will be required to prevent damage to the adjoining structures.

Given the ground conditions encountered, suitable retention systems would be including a contiguous pile wall (where the gaps between piles progressively filled with grout / concrete) or secant pile walls. Although the choice of support should be discussed with an experienced contractor and will primarily depend on cost, although other factors such as the aesthetics of the final wall, the potential impact of seepage water at the soil/bedrock interface and whether it can function as a structural support for foundations.

For a piled wall option, concrete or grout injected continuous flight auger (CFA) piles are recommended as the sand profile can collapse, particularly where seepage water is encountered. Sheet piling or driven steel piles is not normally recommended because of



the potential to adversely affect nearby structures due to the ground vibration generated during installation.

The design of the earth retaining structure should be designed by a suitably experienced structural engineer in accordance with AS4678-2002 Earth Retaining Structures (reference 11) with consideration of both the short- and long-term configurations. In the short term, should the shoring walls be cantilevered or supported by a single row of anchors and some movement behind the walls can be tolerated, earth pressures acting on the shoring walls can be calculated using a triangular earth pressure distribution calculated using an 'active' earth pressure coefficient.

When internal props, such as the ground floor slab, restrain retaining wall movement, or where significant movements cannot be tolerated (rigid wall) such as adjacent to adjoining structures, an 'at-rest' earth pressure coefficient (K_0) should be adopted with either a uniform or trapezoidal pressure distribution. It should be noted that shoring which is designed for this 'at rest' coefficient will still undergo some lateral movements, depending on the final configuration of the wall and construction sequence. Additionally, a factor of safety should be applied in considerations of the wall movement needed to fully mobilise passive pressure. Passive restraint in the soil profile below the basement level can be designed based on a passive earth pressure coefficient (K_p).

The design of any retaining structures should make allowance for all applicable surcharge loadings including construction activities around the perimeter of the excavation and adjacent buildings. Consideration should be given to the possibility of a hydrostatic pressure due to build-up of water behind the wall (e.g. from broken services), unless permanent subsurface drainage can be provided.

Finally, computer aided analysis may be carried out to assess potential ground movements based on different wall designs and construction sequence, so as to control deflections to within tolerable limits. It is also considered prudent to carry out surveys before and after installation to measure the actual movement of the wall or soil.

Preliminary geotechnical parameters for retaining wall design are provided below in **Table 4**. However, the additional investigations are recommended to confirm the depth, strength and quality of the bedrock formation beneath the entire development.



Table 4: Preliminary Geotechnical Design Parameters – Retaining Walls / Shoring

Material	Unit 1 and 2a Soil	Unit 2b Soil	Unit 3 Sandstone	
Bulk Unit Weight (kN/m ³)	18	19	22	
Earth Pressure Coefficients	Active (K _a) At Rest (K _o) Passive (K _p)	0.33 0.5 3.0	0.27 0.43 3.2	0.3 0.5 3.5
Elastic Modulus (MPa)	5	20	100	
Drained Cohesion c' (kPa)	0	0	40	
Drained Friction Angle ϕ' (°)	30	35	32	
Poisson's Ratio	0.35	0.35	0.3	

Note 1: Unit weights are based on visual assessment only – order of accuracy approximately ±10%.

Note 2: The passive earth pressure coefficients for rock have been reduced to allow for potential defects in the rock mass.

5.2.4 Construction / Excavation Induced Vibration

Structures and utilities adjacent to the excavation area are potentially sensitive to vibrations above certain threshold levels (regarding potential for cracking). When using a hydraulic hammer, vibrations will be transmitted through the ground and potentially impact on adjoining structures. Where possible, the use of other techniques not involving impact (*e.g.* rock saws), should be adopted as they would reduce or possibly eliminate risks of damage due to vibrations.

Where vibration intensive works such as hydraulic hammering of competent rock is proposed, contractors should assess the potential impact of their works based on the borehole logs and local knowledge of similar bedrock formations. Monitoring of construction induced vibration should be undertaken at the commencement of such activities at the nearest vibration receptor and in consultation with the project superintendent and geotechnical engineer so that excessive vibration effects are not generated.

Peak Particle Velocity (PPV) is usually the adopted measure of ground vibration, and the safe limits depend on the sensitivity of the adjoining structures. There are several Australian and overseas publications which provide vibration velocity guideline levels (or safe limits) including:



- ◊ Australian Standard AS2187.2-2006 Explosives - Storage and use - Use of explosives - Appendix J: Ground Vibrations and Airblast Overpressure (reference 12).
- ◊ Australian Standard AS2670.2-1990 Evaluation of human exposure to whole-body vibration - Part 2: Continuous and shock-induced vibration in buildings (1 to 80 Hz) (reference 13).
- ◊ DIN 4150 – Part 3 – 1999. Effects if Vibration on Structures (reference 14).
- ◊ Department of Environment and Conservation NSW, 2006. Assessing Vibration: a technical guideline (reference 15).
- ◊ British Standard BS 7385-1:1990. Evaluation and measurement for vibration in buildings. Guide for measurement of vibrations and evaluation of their effects on buildings (reference 16).
- ◊ British Standard BS 7385-2:1993. Evaluation and measurement for vibration in buildings. Guide to damage levels from groundborne vibration (reference 17).

Furthermore, the owners of adjoining assets/utilities sometimes have their own limits. In the absence of PPV guidelines from affected asset owners, GEE recommends that a 5mm/s limit be placed on vibrations for the adjoining residential structures.

If vibration levels are found to be unacceptable during the earthworks, it may be necessary to adopt vibration mitigation measures such as:

- ◊ The use of smaller excavation plant and hydraulic hammers,
- ◊ The use of a rock sawing or grinder adjacent to the site boundaries. GEE notes that this equipment also reduces the possibility of over-break and loosening of the rock mass.
- ◊ Hammering at 50% capacity in short bursts to prevent the build-up of resonant frequencies,
- ◊ The use of low vibration techniques such as rotary grinders or chemical rock splitting,
- ◊ Progressive breakage from open excavated faces,
- ◊ Selective breakage along open joints, where present, and
- ◊ Orientation of the rock hammer pick away from property boundaries and into the existing open excavation.

Finally, human discomfort levels caused by vibration are typically less than the levels that are likely to cause cosmetic or structural damage to structures. Therefore, complaints



may be lodged by neighbours before any cosmetic or structural damage occurs. In this regard, consideration may be given to adopting more stringent vibration limits recommended for human amenity or, as a minimum, ensuring that vibration monitoring is undertaken as reassurance to confirm that vibrations are within safe limits. Acceptable vibration limits for human comfort caused by construction and excavation equipment are provided in DEC (2006) (reference 15). Specifically, maximum acceleration limits as specified in Table 2.2 of the guideline should be adopted.

5.3 SALINITY RISK

The lab testing completed herein indicates that the soil profile is non-saline and therefore a site-specific salinity management plan is not warranted.

5.4 FOUNDATIONS

Following the required excavation work for the proposed basement levels, the subgrade is expected to comprise the sandstone bedrock formation. The shoring piles, if doubling as foundations, will also extend well into the sandstone formation.

The sandstone bedrock formation can provide a minimum allowable end bearing capacity of 800kPa (reference 18). However, additional investigation is recommended post demolition to confirm the depth, strength and quality of the bedrock beneath the entire development, which in turn will allow better design parameters for the foundations. As previously mentioned, grout or concrete injected Continuous Flight Auger (CFA) piles are recommended as the sandy soil has the potential to collapse. Particularly if seepage water is encountered at the soil and bedrock interface.

Finally, footing systems should be designed by a suitably qualified and experienced structural engineer, and GEE recommends that inspection by a geotechnical engineer is undertaken during the footing excavation stage, to confirm that the design founding conditions have been achieved.

5.4.1 Aggressivity / Exposure Classification

Based on the limited exposure classification test results (Section 4.2.2), and in accordance with AS 2159-2009 (reference 8), the subsurface concrete structures (*e.g.* footings) should be designed based on non-aggressive soil conditions for concrete. According to Australian Standard AS 3600-2009 (reference 9), the equivalent exposure classification is 'A1'. With respect to unprotected steel, the natural soil profile is considered to be non-aggressive / non-corrosive.



6 CONCLUSION AND RECOMMENDATIONS

GEE considers that sufficient information has been gained to be confident of the subsurface conditions across the site and to provide Council with assurances regarding the geotechnical feasibility of the proposed development.

Based on the results of the investigation, the proposed development is considered feasible, and GEE concludes that the bedrock formation beneath the site can withstand the proposed loads to be imposed, and standard shoring works (provided they are designed by a structural engineer), will ensure the stability of the excavation and provide protection and support of the adjoining properties, subject to engineering design and the recommendations of this report being properly implemented. Notwithstanding this additional investigation is recommended to confirm that the subsurface conditions encountered at the rear of the site are consistent with the front of the site. Preferably these investigations are completed post demolition of the existing structures to allow better access to the entire site.

GEE will be pleased to assist with any further advice or geotechnical services required in regard to the proposed development.



7 GENERAL LIMITATIONS

Soil and rock formations are variable. The logs or other information presented as part of this report indicate the approximate subsurface conditions only at the specific test locations. Boundaries between zones on the logs or stratigraphic sections are often not distinct, but rather are transitional and have been interpreted.

The precision with which subsurface conditions are indicated depends largely on the frequency and method of sampling, and on the uniformity of subsurface conditions. The spacing of test sites also usually reflects budget and schedule constraints. Groundwater conditions described in this report refer only to those observed at the place and under circumstances noted in the report. The conditions may vary seasonally or as a consequence of construction activities on the site or adjacent sites.

Where ground conditions encountered at the site differ significantly from those anticipated in the report, either due to natural variability of subsurface conditions or construction activities, it is a condition of this report that GEE be notified of any variations and be provided with an opportunity to review the recommendations of this report. Recognition of changed soil and rock conditions requires experience and it is recommended that a suitably experienced geotechnical engineer be engaged to visit the site with sufficient frequency to detect if conditions have changed significantly.

The comments given in this report are intended only for the guidance of the design engineer, or for other purposes specifically noted in the report. The number of boreholes or test excavations necessary to determine all relevant underground conditions which may affect construction costs, techniques and equipment choice, scheduling, and sequence of operations would normally be greater than has been carried out for design purposes. Contractors should therefore rely on their own additional investigations, as well as their own interpretations of the borehole data in this report, as to how subsurface conditions may affect their work.



8 REFERENCES

1. Crozier Geotechnical Consultants, 2018: *Report on Geotechnical Site Investigation for Proposed Residential Development at 671-679 Old South Head Road, Vaucluse*. Prepared for OSHR Holdings at Vaucluse Pty Ltd. Project No. 2018-106 Dated August 2018.
2. Department of Mineral Resources, 1983: Sydney 1:100,000 *Geological Series Map Sheet 9130 (Edition 1)*.
3. Department of Environment, Climate Change and Water, 2009: *Sydney 1:100 000 Soil Landscape Series Sheet 9130 (fourth edition)*.
4. DLWC, 1997: Department of Land and Water Conservation of NSW, 1997: *Sydney Heads Acid Sulfate Soil Risk Map – Edition Two*.
5. Australian Standards, 1997. *AS1289.6.3.1 Methods of testing soils for engineering purposes – Soil strength and consolidation tests – Determination of the penetration resistance of a soil – Standard Penetration Test (SPT)*.
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7. Department of Land and Water Conservation NSW, 2002: *Site investigations for urban salinity*.
8. Australian Standard (AS) 2159 -2009: Piling Design and Installation
9. Australian Standard (AS) 3600 – 2009: Concrete Structures.
10. New South Wales Environment Protection authority (NSW EPA), 2014: *Waste classification guidelines – Part 1 classifying waste*. November 2014.
11. Australian Standard AS4678-2002: Australian Standard, 2002: *Earth Retaining Structures*.
12. Australian Standard AS2187.2-2006 *Explosives - Storage and use - Use of explosives - Appendix J: Ground Vibrations and Airblast Overpressure*.
13. Australian Standard AS2670.2-1990: *Evaluation of human exposure to whole-body vibration - Part 2: Continuous and shock-induced vibration in buildings (1 to 80 Hz)*.
14. DIN 4150 – Part 3 – 1999. *Effects of Vibration on Structures*.
15. Department of Environment and Conservation NSW, 2006. *Assessing Vibration: a technical guideline*.

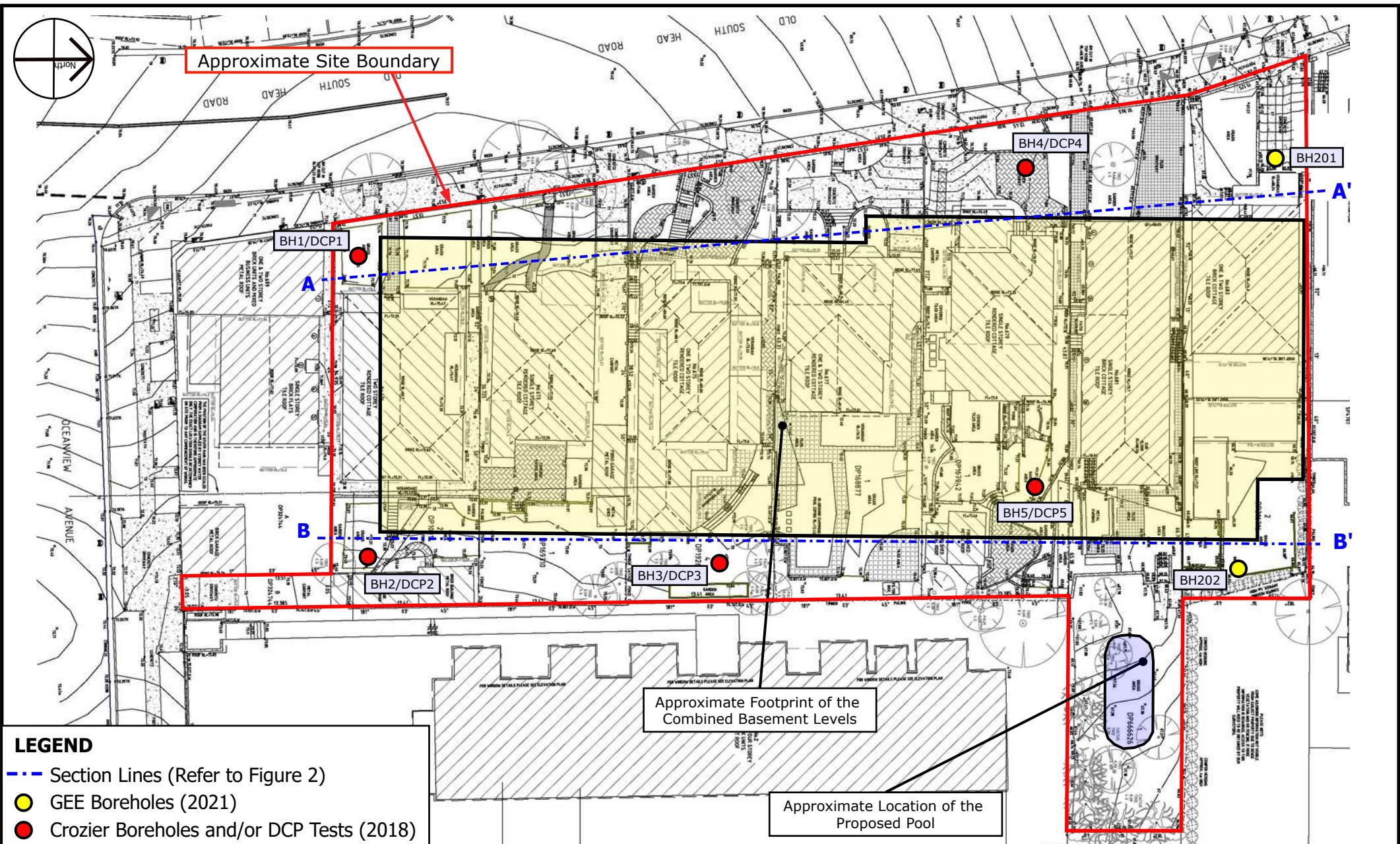


16. British Standard BS 7385-1:1990. *Evaluation and measurement for vibration in buildings. Guide for measurement of vibrations and evaluation of their effects on buildings.*
17. British Standard BS 7385-2:1993. *Evaluation and measurement for vibration in buildings. Guide to damage levels from groundborne vibration.*
18. Pells et al, 2019: *Classification of Sandstones and Shale in the Sydney Region: A Forty Year Review*. Australian Geomechanics Society, 2019.



FIGURES

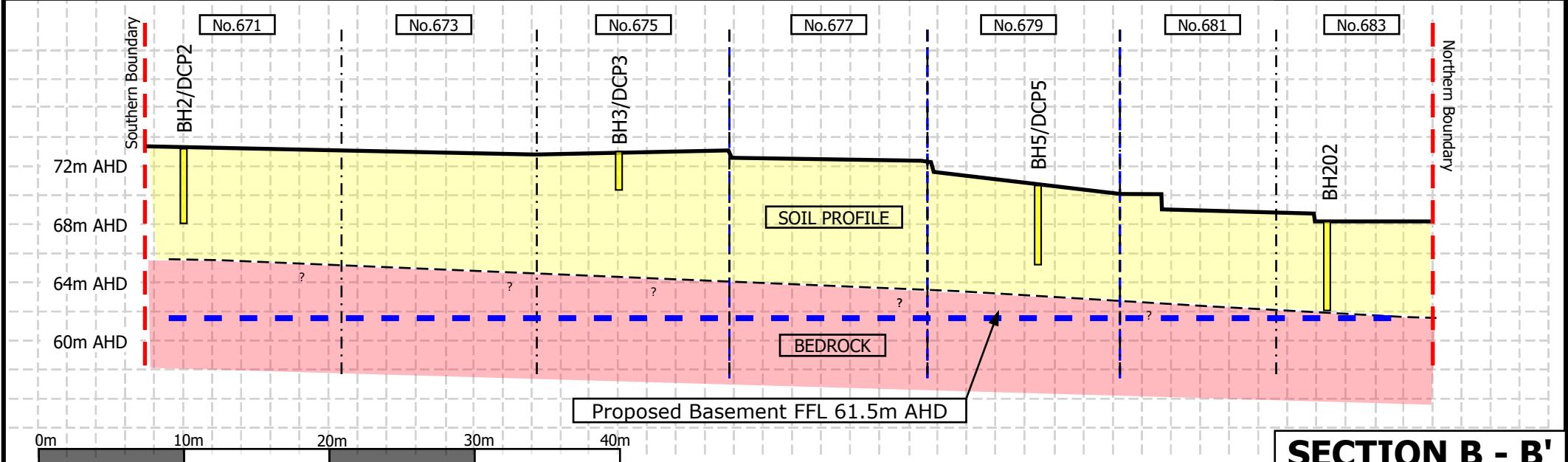
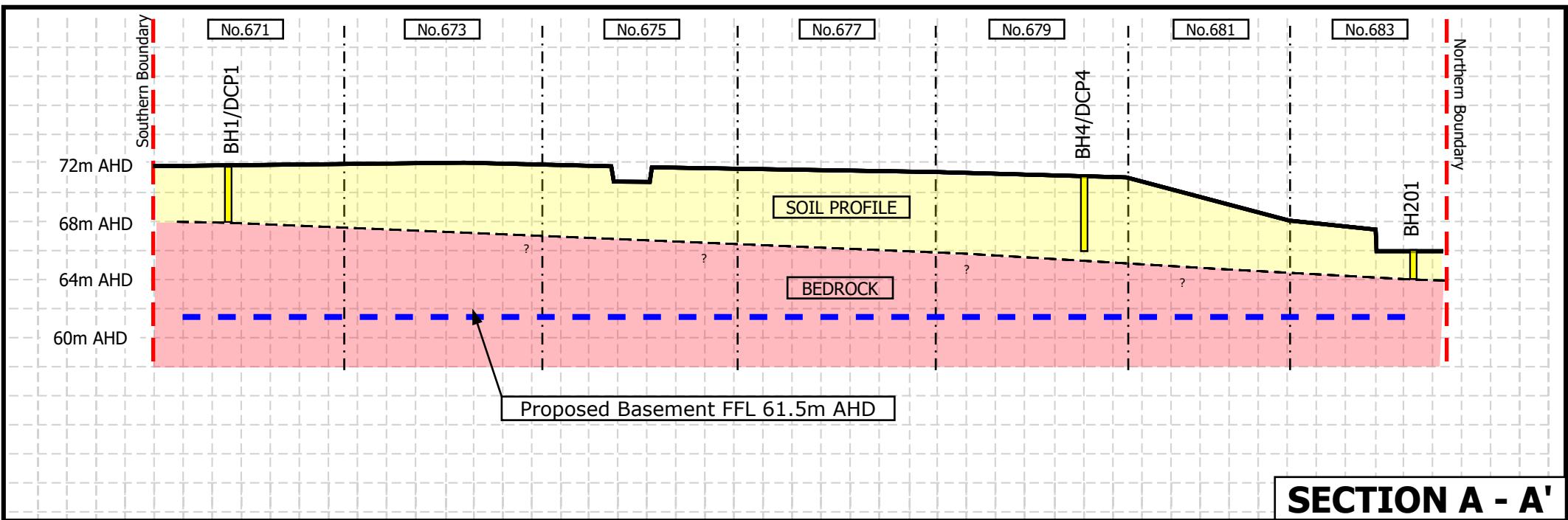
- 1 – Site Plan
- 2 – Site Sections A-A' and B-B'



LEGEND

- Section Lines (Refer to Figure 2)
- GEE Boreholes (2021)
- Crozier Boreholes and/or DCP Tests (2018)

Base Image: Plan Showing Detail and Levels Over Lot 2 DP10314 - Lot 1 DP167942 Being 671-679 Old South Head Road Vaucluse. Prepared by Survplan Drawing 1308CO_MHN Revision B Dated 12.04.21

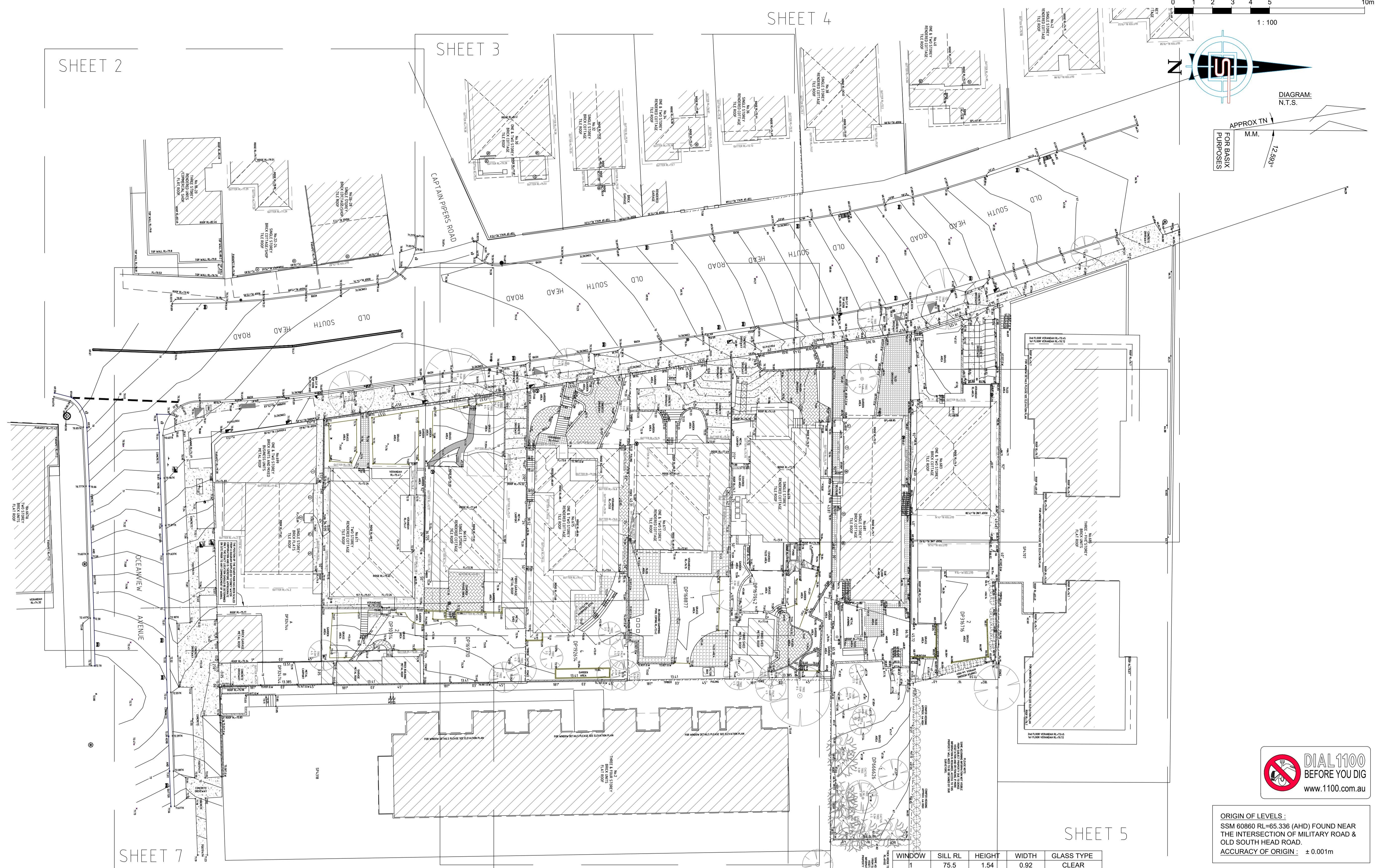


Geotechnical investigation Report
671 - 683 Old South Head Road, Vaucluse Bay NSW



APPENDIX A
SURVEY AND ARCHITECTURAL PLANS (44 SHEETS)

SHEET 2



ABN 83 914 413 296
 PO BOX 242 HELENSBURGH NSW 2508
 PH 0420 944 413 Email: mail@survplan.com.au

PLAN SHOWING DETAIL AND LEVELS
 OVER LOT 2 DP10314 - LOT 1 DP167942
 BEING No.671-679 OLD SOUTH HEAD RD
 VAUCLUSE FOR DESIGN PURPOSES
 AND TO SUPPORT A
 DEVELOPMENT APPLICATION

Rev.	Amendments	Date
A	ADJ BUILDING DESCRIPTION	17.09.18
B	ADDITIONAL SURVEY INFORMATION	12.04.21

JOB No.	YOUR REF:
1208	MEISSEN PROPERTIES
DRAWING No.	CLIENT:
1308CO_MHN.dwg	MHN DESIGN UNION
SCALE: 1:250 (A1)	SURVEYED: M.S. DRAWN: M.S. CHECKED: M.S.
DATUM: A.H.D.	DATE: 5.12.17
PHOTOCOPY	DATE: 11.12.17
DEVELOPMENT APPLICATION	DATE: 14.12.17

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VAUGHAN WADY
 REGISTERED SURVEYOR #8684

Surveyor Registered under the Surveying and Spatial Information Act 2002

AREA LOT B VIDE DP 324744: 37.9 m ² BY CALC: 40.98 m ²	AREA LOT 4 VIDE DP 192614: 524.8 m ² BY CALC: 528.4 m ²
AREA LOT 2 VIDE DP 10314: 474.2 m ² BY CALC: 480.3 m ²	AREA LOT 1 VIDE DP 316877: 550.1 m ² BY CALC: 552.4 m ²
AREA LOT 2 VIDE DP 316716: 550.1 m ² BY CALC: 550.5 m ²	AREA LOT 2 VIDE DP 316716: 550.1 m ² BY CALC: 550.5 m ²
AREA LOT 1 VIDE DP 169310: 499.5 m ² BY CALC: 504.3 m ²	AREA LOT 1 VIDE DP 167942: 569.1 m ² BY CALC: 573.2 m ²
AREA LOT 1 VIDE DP 666626: 670.2 m ² BY CALC: 678.0 m ²	AREA LOT 1 VIDE DP 666626: 670.2 m ² BY CALC: 678.0 m ²

WINDOW	SILL RL	HEIGHT	WIDTH	Glass Type
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2	73.01	1.1	1.07	CLEAR
3	72.1	2.05	0.85	DOOR
4	73.01	1.1	1.1	CLEAR
5	73.01	1.1	1.2	CLEAR
6	69.8	2.1	1.1	DOOR
7	71.72	1.46	2.8	CLEAR
8	71.72	1.46	2.8	CLEAR
9	71.0	2.18	1.9	CLEAR
10	71.0	2.18	1.9	CLEAR
11	70.83	2.5	4.53	CLEAR
12	70.83	2.5	4.53	CLEAR
13	70.99	2.28	7.96	CLEAR
14	73.87	1.2	2	CLEAR
15	77.3	1.6	1.9	CLEAR
16	77.3	1.6	1.9	CLEAR
17	74.18	0.94	2.18	CLEAR
18	73.3	1.14	1.2	CLEAR
19	71.97	1.24	1	CLEAR
20	73.07	1.22	2.16	CLEAR
21	73.07	1.22	2.16	CLEAR

ORIGIN OF LEVELS :
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 ACCURACY OF ORIGIN : ± 0.001m



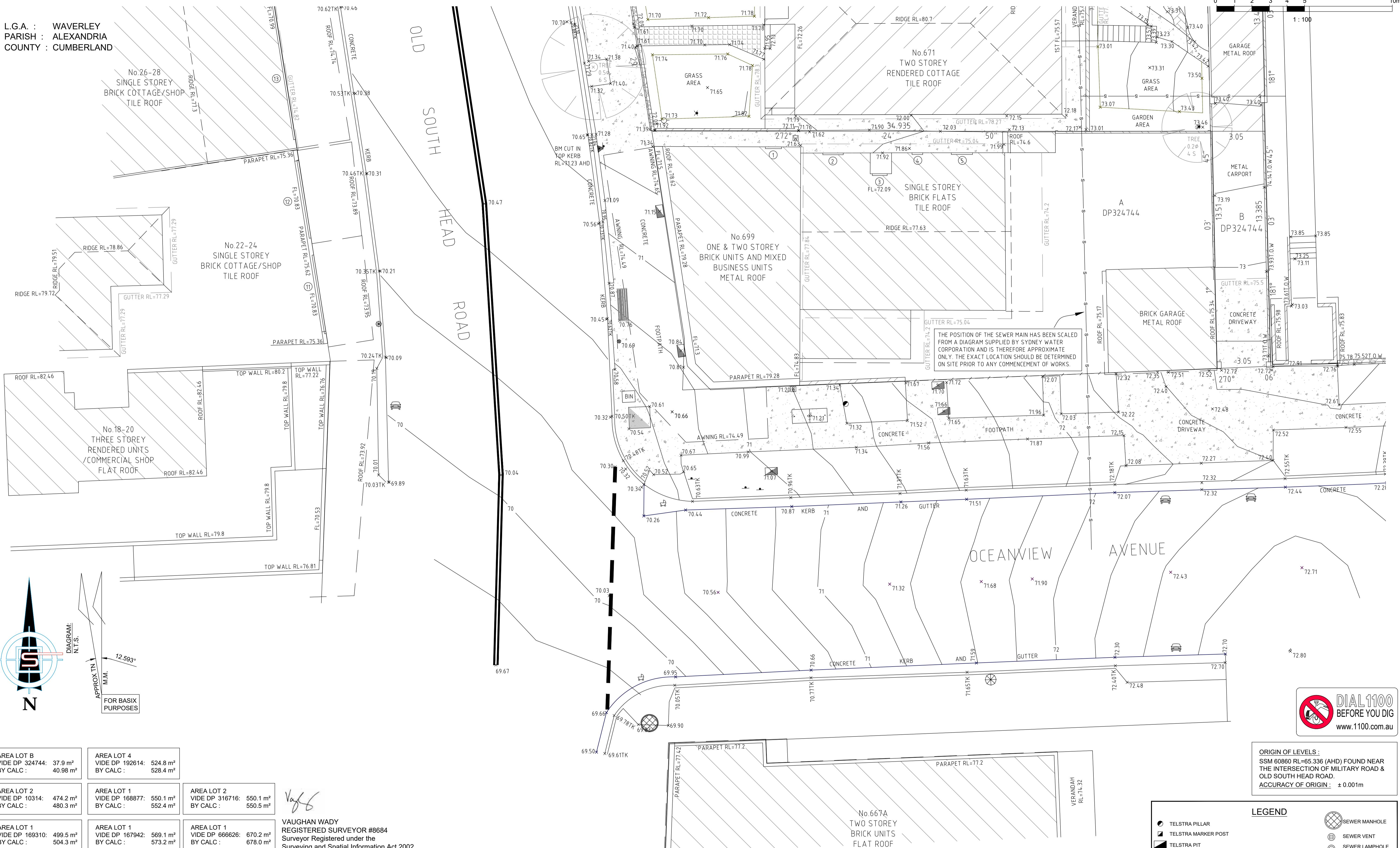
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LEGEND

● TELSTRA PILLAR	SEWER MANHOLE
■ TELSTRA MARKER POST	SEWER VENT
■ TELSTRA PIT	SEWER LAMPOLLE
● POWER POLE	POWER LINE
■ ELECTRICAL PILLAR	POWER POLE
● LIGHT POLE	LIGHT POLE
● GAS METER	GAS METER
□ GAS DIRECTION MARKER	GAS DIRECTION MARKER
W WATER MAIN	WATER MAIN
H HYDRANT	HYDRANT
R RECYCLED WATER	RECYCLED WATER
○ WATER METER	WATER METER
● STOP VALVE	STOP VALVE
✖ WATER TAP	WATER TAP
E	OVERHEAD ELECTRICITY LINE
S	OVERHEAD TELECOM LINE
—	SEWER LINE

A1

L.G.A. : WAVERLEY
PARISH : ALEXANDRIA
COUNTY : CUMBERLAND



AREA LOT B
VIDE DP 324744: 37.9 m²
BY CALC : 40.98 m²

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BY CALC : 552.4 m²

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VIDE DP 169310: 499.5 m²
BY CALC : 504.3 m²

AREA LOT 1
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BY CALC : 573.2 m²

AREA LOT 1
VIDE DP 316716: 550.1 m²
BY CALC : 550.5 m²

SURVPLAN
SURVEYING / PLANNING / DESIGN
ABN 83 914 413 296
PO BOX 242 HELENSBURGH NSW 2508
PH 0420 944 413 Email: mail@survplan.com.au

PLAN SHOWING DETAIL AND LEVELS
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VAUCLEUSE FOR DESIGN PURPOSES
AND TO SUPPORT A
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Rev. Amendments Date
A ADJ BUILDING DESCRIPTION 17.09.18
B ADDITIONAL SURVEY INFORMATION 12.04.21

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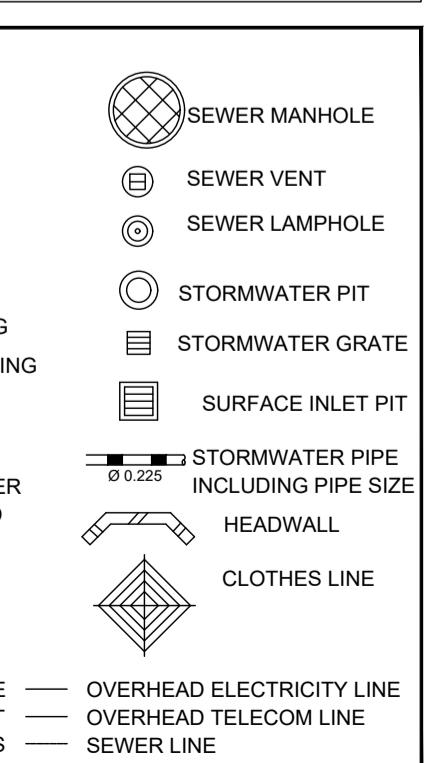
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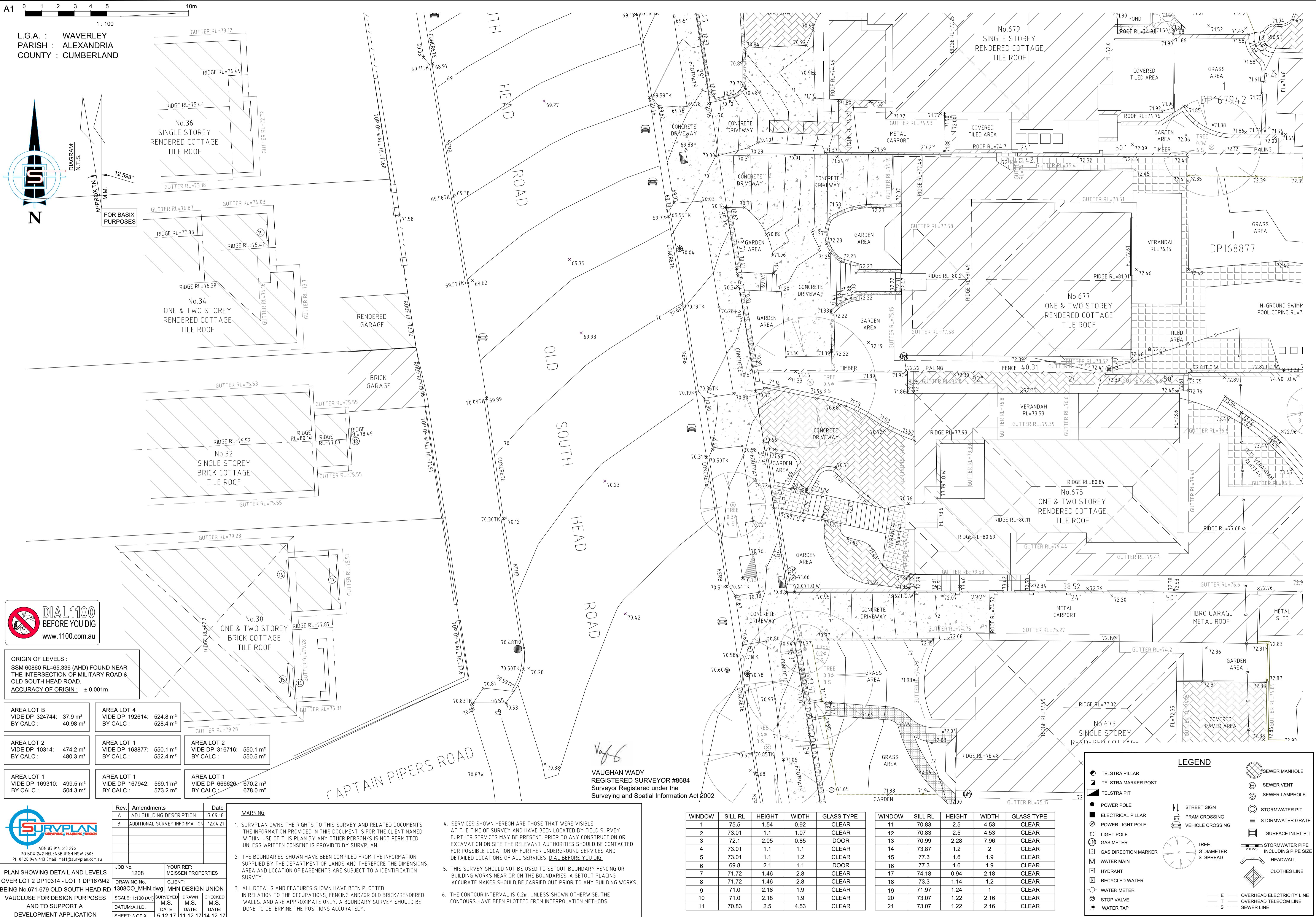
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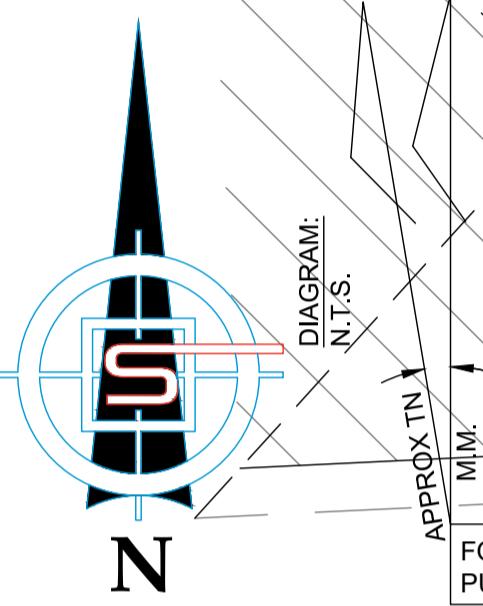
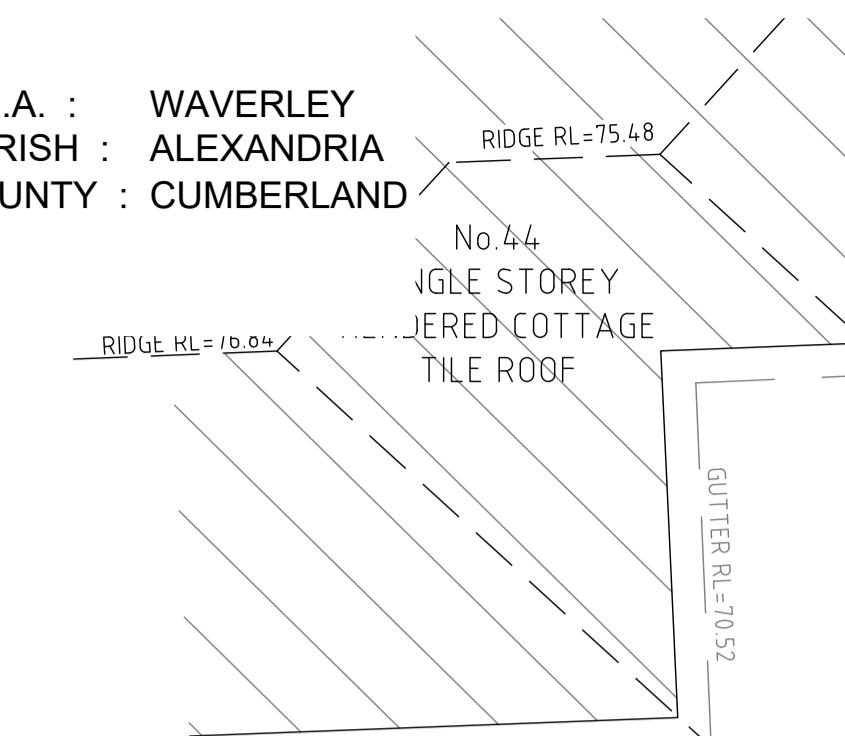
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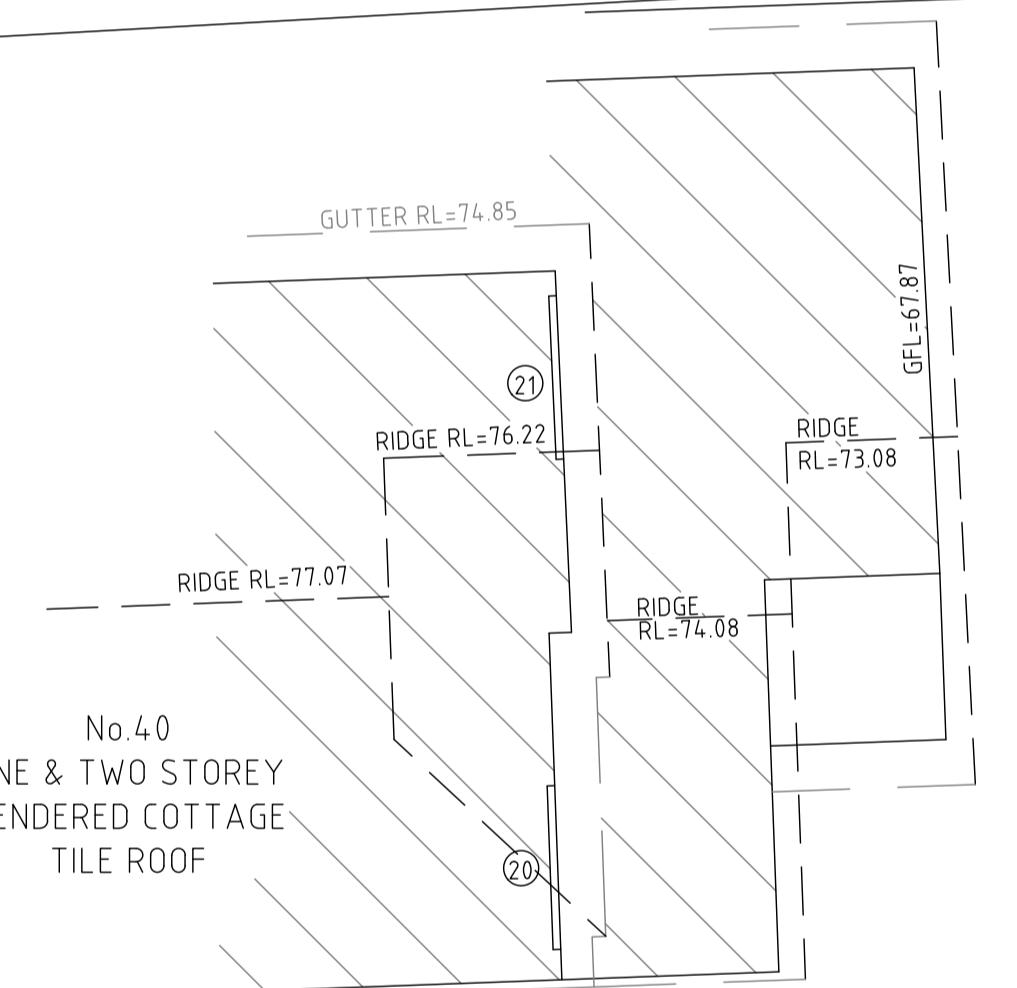


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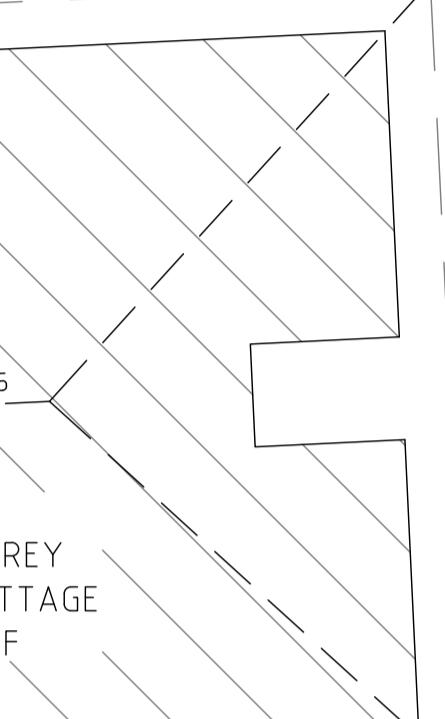
L.G.A. : WAVERLEY
 PARISH : ALEXANDRIA
 COUNTY : CUMBERLAND



No.40
ONE & TWO STOREY
RENDERED COTTAGE
TILE ROOF



No.42
SINGLE STOREY
RENDERED COTTAGE
TILE ROOF



No.44
SINGLE STOREY
RENDERED COTTAGE
TILE ROOF

VAG
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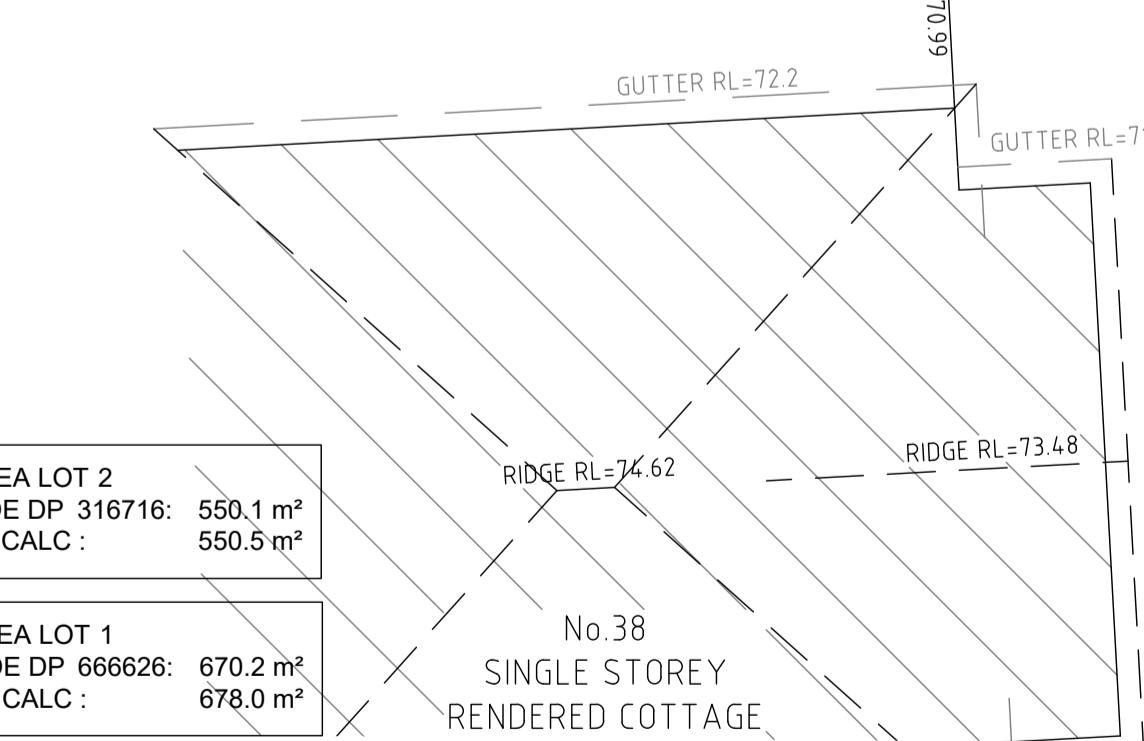
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No.38
SINGLE STOREY
RENDERED COTTAGE



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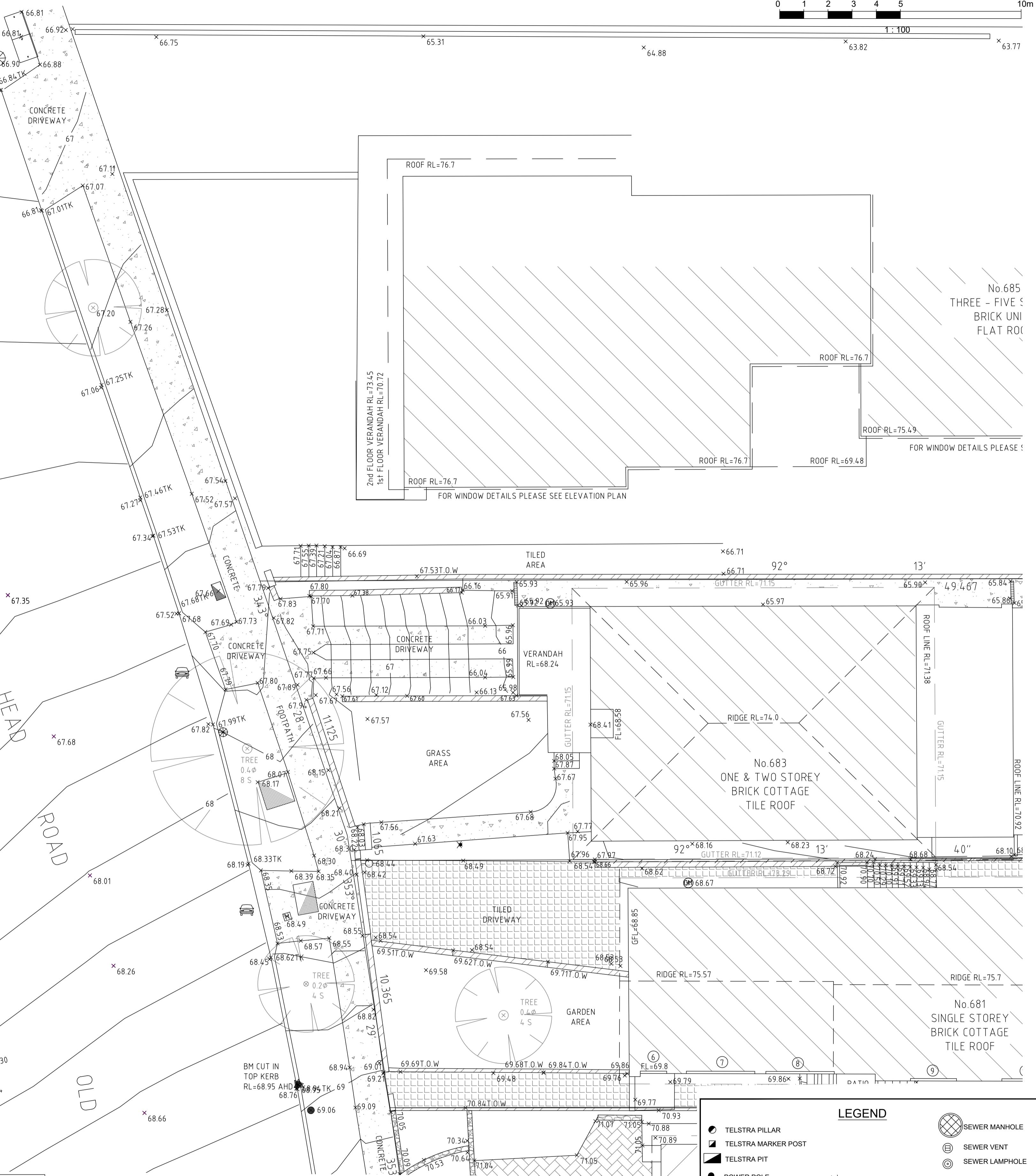
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Rev. Amendments Date
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 B ADDITIONAL SURVEY INFORMATION 12.04.21

JOB No. 1208 YOUR REF: MEISSEN PROPERTIES
 DRAWING No. 1308CO_MHN.dwg CLIENT: MHN DESIGN UNION
 SCALE: 1:100 (A1) SURVEYED M.S. DRAWN M.S. CHECKED M.S.
 DATUM: A.H.D. DATE: 11.12.17 14.12.17

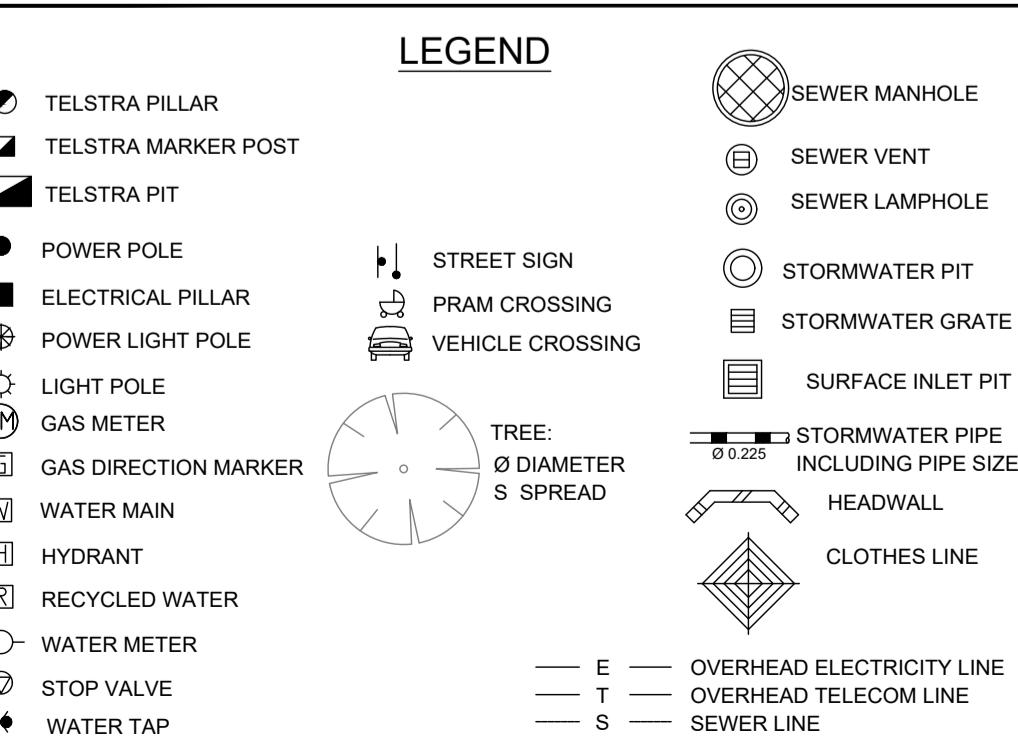
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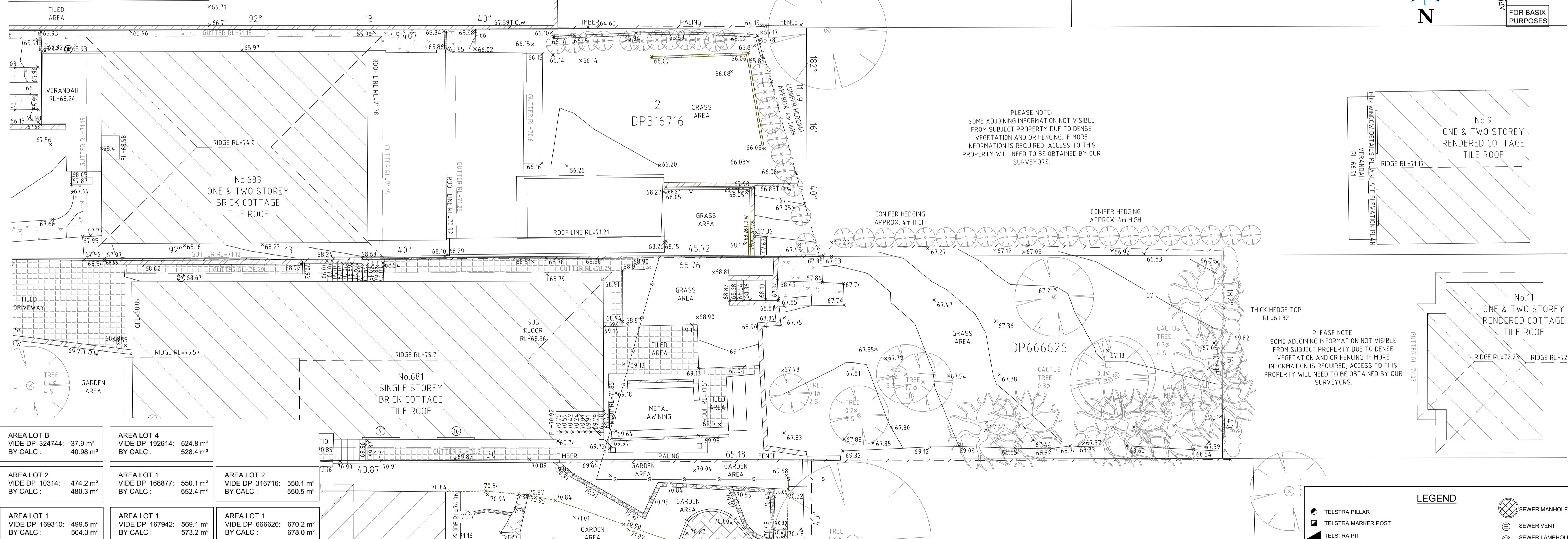
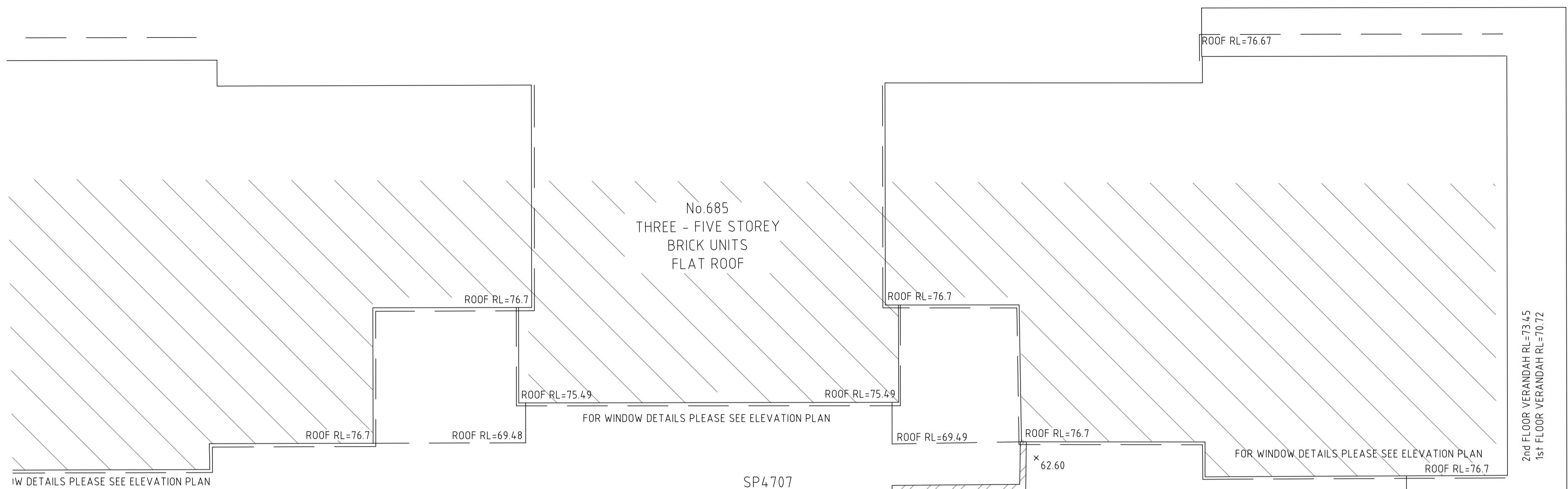
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14	73.87	1.2	2	CLEAR
15	77.3	1.6	1.9	CLEAR
16	77.3	1.6	1.9	CLEAR
17	74.18	0.94	2.18	CLEAR
18	73.3	1.14	1.2	CLEAR
19	71.97	1.24	1	CLEAR
20	73.07	1.22	2.16	CLEAR
21	73.07	1.22	2.16	CLEAR



VW
VAUGHAN WADY
REGISTERED SURVEYOR #8684
Surveyor Registered under the
Surveying and Spatial Information Act 2002

ORIGIN OF LEVELS:
SSM 60860 RL=65.336 (AHD) FOUND NEAR
THE INTERSECTION OF MILITARY ROAD &
OLD SOUTH HEAD ROAD.
ACCURACY OF ORIGIN: ± 0.001m



AREA LOT B
VIDE DP 324744: 37.9 m²
BY CALC: 40.98 m²

AREA LOT 4
VIDE DP 192614: 524.8 m²
BY CALC: 528.4 m²

AREA LOT 2
VIDE DP 10214: 474.2 m²
BY CALC: 480.3 m²

AREA LOT 1
VIDE DP 168877: 550.1 m²
BY CALC: 552.4 m²

AREA LOT 1
VIDE DP 169310: 499.5 m²
BY CALC: 504.3 m²

AREA LOT 1
VIDE DP 167942: 569.1 m²
BY CALC: 573.2 m²

Rev. Amendments Date
A ADJ BUILDING DESCRIPTION 17.09.18
B ADDITIONAL SURVEY INFORMATION 12.04.21

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PLAN SHOWING DETAIL AND LEVELS
OVER LOT 2 DP 10314 - LOT 1 DP167942
BEING No.671-679 OLD SOUTH HEAD RD
VAUCLEUSE FOR DESIGN PURPOSES
AND TO SUPPORT A
DEVELOPMENT APPLICATION

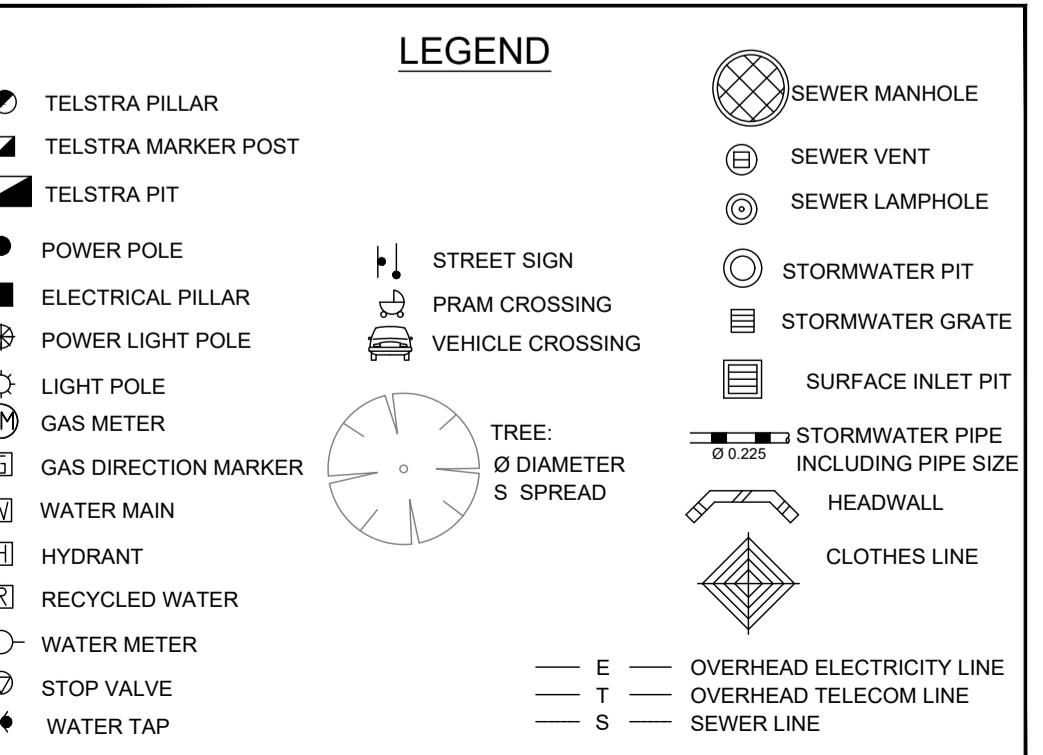
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DRAWING No. 1308CO_MHN.dwg CLIENT: MHN DESIGN UNION
SCALE: 1:100 (A1) SURVEYED M.S. DRAWN M.S. CHECKED M.S.
DATUM: A.H.D. DATE: 5.12.17 DATED: 11.12.17 14.12.17

ABN 83 914 413 296
PO BOX 242 HELENSBURGH NSW 2508
PH 02 42 444 413 Email: mail@survplan.com.au

SHEET: 5 of 9

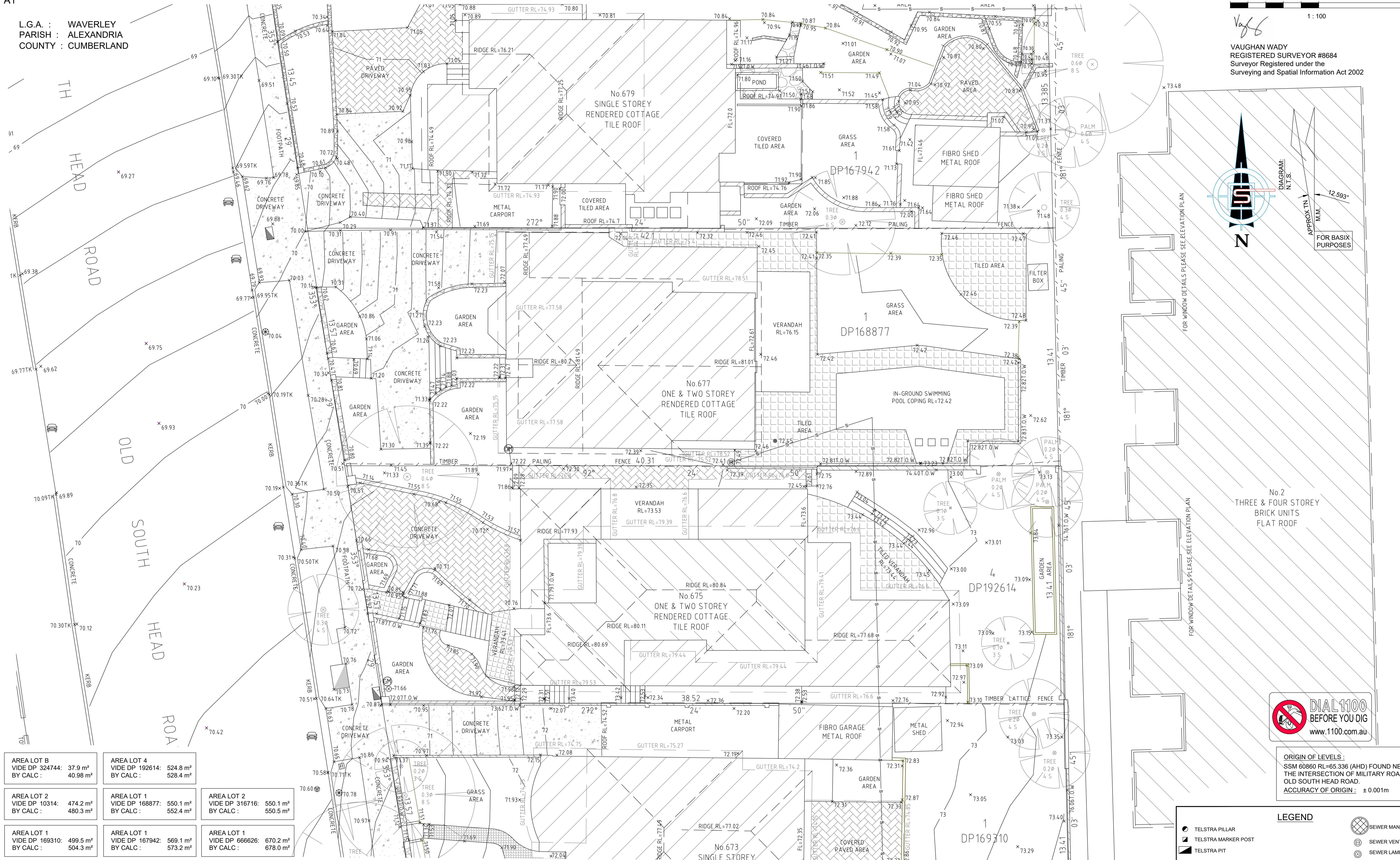
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2	73.01	1.1	1.07	CLEAR
3	72.1	2.05	0.85	DOOR
4	73.01	1.1	1.1	CLEAR
5	73.01	1.1	1.2	CLEAR
6	69.8	2.1	1.1	DOOR
7	71.72	1.46	2.8	CLEAR
8	71.72	1.46	2.8	CLEAR
9	71.0	2.18	1.9	CLEAR
10	71.0	2.18	1.9	CLEAR
11	70.83	2.5	4.53	CLEAR

WINDOW	SILL RL	HEIGHT	WIDTH	Glass Type
11	70.83	2.5	4.53	CLEAR
12	70.83	2.5	4.53	CLEAR
13	70.99	2.28	7.96	CLEAR
14	73.87	1.2	2	CLEAR
15	77.3	1.6	1.9	CLEAR
16	77.3	1.6	1.9	CLEAR
17	74.18	0.94	2.18	CLEAR
18	73.3	1.14	1.2	CLEAR
19	71.97	1.24	1	CLEAR
20	73.07	1.22	2.16	CLEAR
21	73.07	1.22	2.16	CLEAR



A1

L.G.A. : WAVERLEY
PARISH : ALEXANDRIA
COUNTY : CUMBERLAND



AREA LOT B
VIDE DP 324744: 37.9 m²
BY CALC: 40.98 m²

AREA LOT 4
VIDE DP 192614: 524.8 m²
BY CALC: 528.4 m²

AREA LOT 2
VIDE DP 10314: 474.2 m²
BY CALC: 480.3 m²

AREA LOT 1
VIDE DP 168877: 550.1 m²
BY CALC: 552.4 m²

AREA LOT 1
VIDE DP 169310: 499.5 m²
BY CALC: 504.3 m²

AREA LOT 1
VIDE DP 167942: 569.1 m²
BY CALC: 573.2 m²

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PLAN SHOWING DETAIL AND LEVELS
OVER LOT 2 DP10314 - LOT 1 DP167942
BEING NO.671-679 OLD SOUTH HEAD RD
VAUCLEUSE FOR DESIGN PURPOSES
AND TO SUPPORT A
DEVELOPMENT APPLICATION

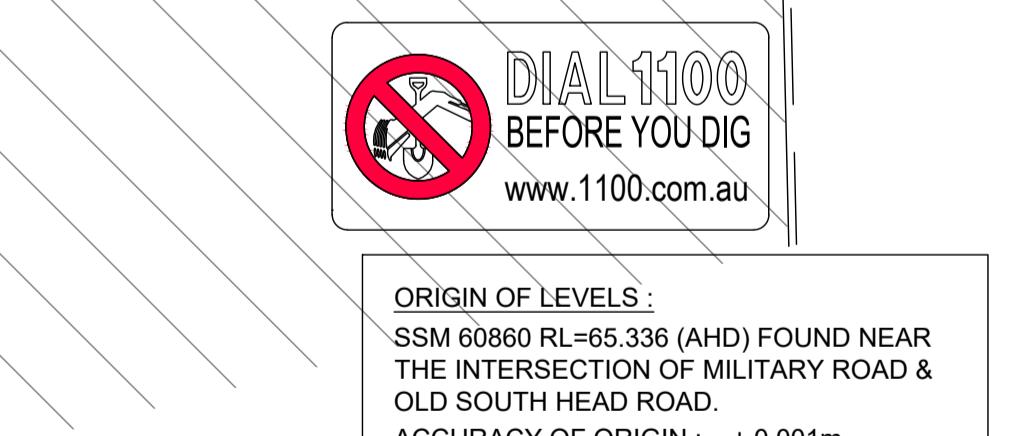
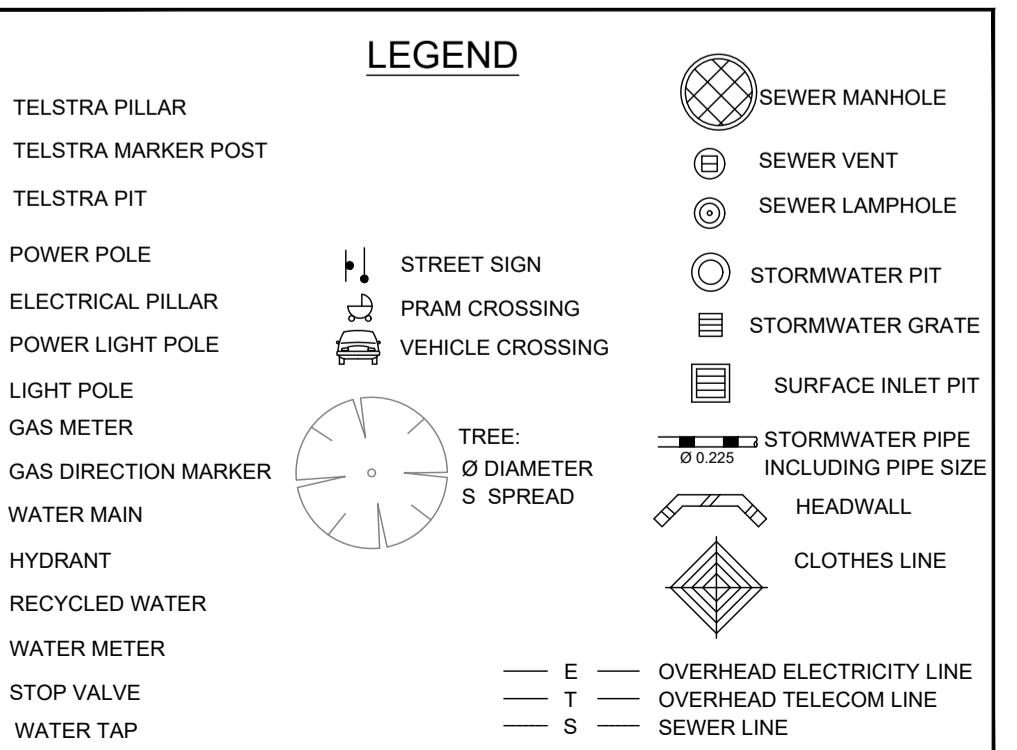
Rev. Amendments Date
A ADJ BUILDING DESCRIPTION 17.09.18
B ADDITIONAL SURVEY INFORMATION 12.04.21

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DRAWING No. 1308CO_MHN.dwg CLIENT: MHN DESIGN UNION
SCALE: 1:100 (A1) SURVEYED M.S. DRAWN M.S. CHECKED M.S.
DATUM: A.H.D. DATE: 5.12.17 DATED: 11.12.17 14.12.17
SHEET: 6 OF 9

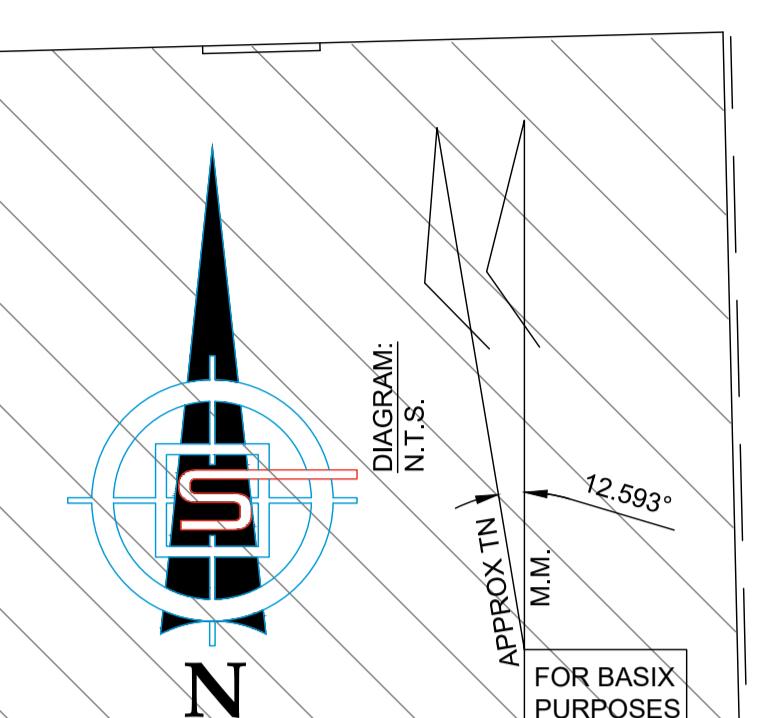
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WINDOW	SILL RL	HEIGHT	WIDTH	Glass Type
1	75.5	1.54	0.92	CLEAR
2	73.01	1.1	1.07	CLEAR
3	72.1	2.05	0.85	DOOR
4	73.01	1.1	1.1	CLEAR
5	73.01	1.1	1.2	CLEAR
6	69.8	2.1	1.1	DOOR
7	71.72	1.46	2.8	CLEAR
8	71.72	1.46	2.8	CLEAR
9	71.0	2.18	1.9	CLEAR
10	71.0	2.18	1.9	CLEAR
11	70.83	2.5	4.53	CLEAR

WINDOW	SILL RL	HEIGHT	WIDTH	Glass Type
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16	77.3	1.6	1.9	CLEAR
17	74.18	0.94	2.18	CLEAR
18	73.3	1.14	1.2	CLEAR
19	71.97	1.24	1	CLEAR
20	73.07	1.22	2.16	CLEAR
21	73.07	1.22	2.16	CLEAR



0 1 2 3 4 5 10m
1 : 100
VW
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REGISTERED SURVEYOR #8684
Surveyor Registered under the
Surveying and Spatial Information Act 2002



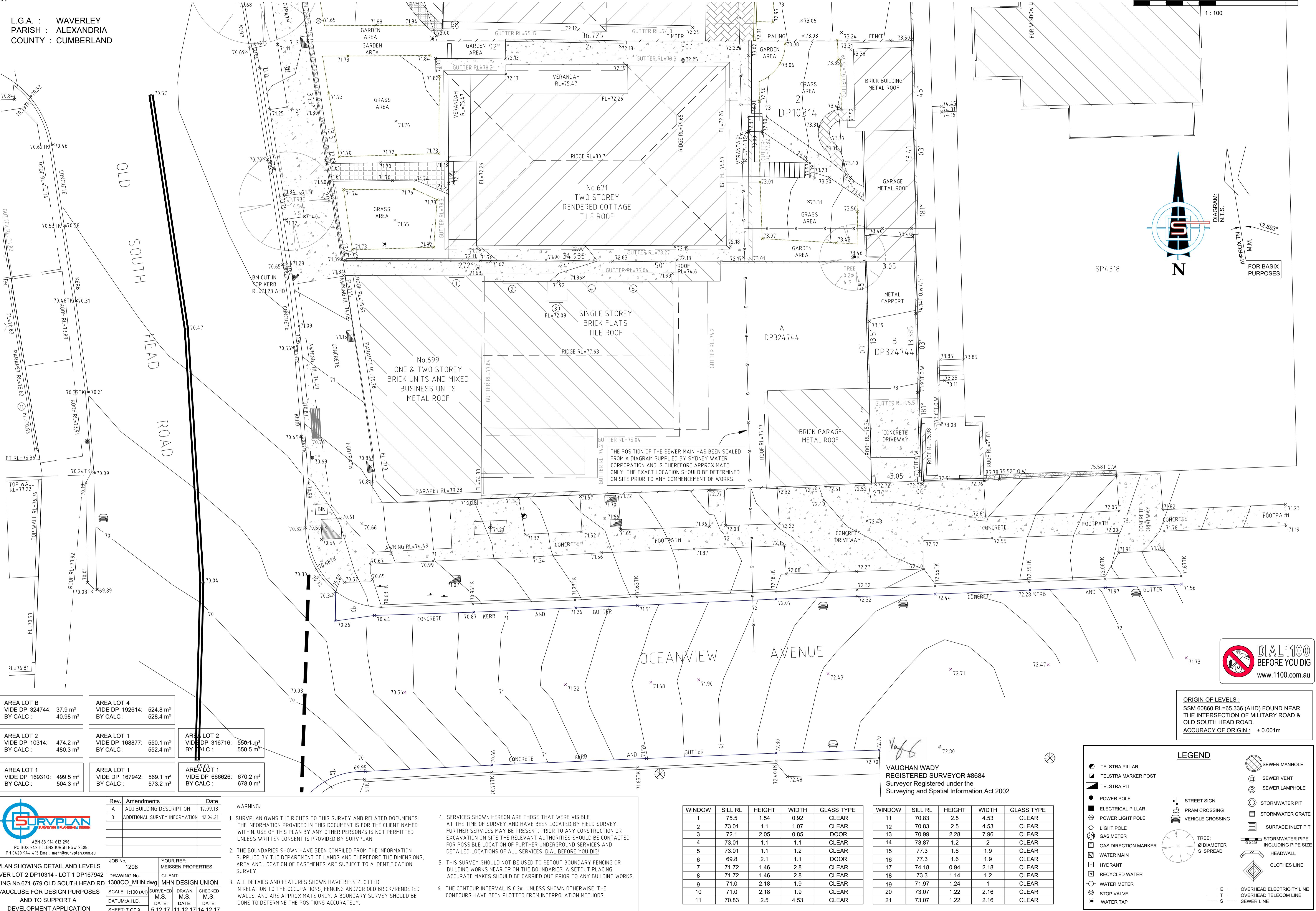
FOR WINDOW DETAILS PLEASE SEE ELEVATION PLAN

FOR FENCE DETAILS PLEASE SEE ELEVATION PLAN

FOR GARDEN AREA DETAILS PLEASE SEE ELEVATION PLAN

A1

L.G.A. : WAVERLEY
PARISH : ALEXANDRIA
COUNTY : CUMBERLAND



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Drawing List				
Sheet Number	Sheet Series	Sheet Name	Sheet Status	Current Revision
A00.000	A00	COVER PAGE - DRAWING LIST	DA ISSUE	A
A00.001	A00	EXTERNAL PERSPECTIVE 01	DA ISSUE	A
A00.002	A00	EXTERNAL PERSPECTIVE 02	DA ISSUE	A
A00.003	A00	EXTERNAL PERSPECTIVE 03	DA ISSUE	A
A00.004	A00	EXTERNAL PERSPECTIVE 04	DA ISSUE	A
A01.001	A01	SITE PLAN	DA ISSUE	A
A01.002	A01	EXISTING CONDITIONS	DA ISSUE	A
A01.003	A01	DEMOLITION	DA ISSUE	A
A03.001	A03	GROUND LOWER PLAN	DA ISSUE	A
A03.002	A03	GROUND UPPER PLAN	DA ISSUE	A
A03.003	A03	LEVEL 01 PLAN	DA ISSUE	A
A03.004	A03	LEVEL 02 PLAN	DA ISSUE	A
A03.005	A03	LEVEL 03 PLAN	DA ISSUE	A
A03.006	A03	ROOF PLAN	DA ISSUE	A
A03.007	A03	BASEMENT 01	DA ISSUE	A
A03.008	A03	BASEMENT 02	DA ISSUE	A
A09.001	A09	BUILDING ELEVATION	DA ISSUE	A
A09.002	A09	BUILDING ELEVATION	DA ISSUE	A
A10.001	A10	BUILDING SECTION	DA ISSUE	A
A10.002	A10	BUILDING SECTION	DA ISSUE	A
A10.003	A10	BUILDING SECTION	DA ISSUE	A
A10.004	A10	BUILDING SECTION	DA ISSUE	A
A10.005	A10	BUILDING SECTION	DA ISSUE	A
A11.001	A11	FACADE TYPE 01	DA ISSUE	A
A11.002	A11	FACADE TYPE 02	DA ISSUE	A
A11.003	A11	FACADE TYPE 03	DA ISSUE	A
A13.001	A13	APARTMENT TYPE - 3B	DA ISSUE	A
A13.002	A13	APARTMENT TYPE - 3B	DA ISSUE	A
A13.003	A13	APARTMENT TYPE - 2B & 1B	DA ISSUE	A
A13.004	A13	APARTMENT TYPE - 3B PENTHOUSE	DA ISSUE	A
A21.001	A21	SHADOW DIAGRAMS - PLAN	DA ISSUE	A
A21.002	A21	SHADOW DIAGRAMS - PERSPECTIVE	DA ISSUE	A
A22.001	A22	AREA PLANS	DA ISSUE	A
A22.002	A22	AREA PLANS	DA ISSUE	A
A22.003	A22	AREA PLANS	DA ISSUE	A
A41.001	A41	MATERIAL SCHEDULE	DA ISSUE	A

Grand total: 36

A 21.10.07 DEVELOPMENT APPLICATION
Rev Date Description SH Initial Checked
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671- 683 OSH RD VAUCLUSE

A00
COVER PAGE - DRAWING LIST

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Scale	@ A1
Drawn	SH Checked
Project No.	S12551
Pilot Date	8/10/2021 12:29:19 AM
BIM	

A00.000 **A**
Revision

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A00
 EXTERNAL PERSPECTIVE 01

Status	CONCEPT
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Drawn	SH Checked
Project No.	S12551
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BIM	
Drawing no.	Revision

A00.001 A

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OLD SOUTH HEAD ROAD
 NORTHERN STREET PERSPECTIVE



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671- 683 OSH RD VAUCLUSE

A00
EXTERNAL PERSPECTIVE 02

Status	CONCEPT
Scale	@ A1
Drawn	SH Checked
Project No.	S12551
Pilot Date	8/10/2021 12:30:04 AM
BIM	
Drawing no.	Revision

A00.002 **A**

OLD SOUTH HEAD ROAD
SOUTHERN STREET PERSPECTIVE

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A00
EXTERNAL PERSPECTIVE 03

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Scale	@ A1
Drawn	SH Checked
Project No.	S12551
Plot Date	8/10/2021 12:30:28 AM
BIM	

Drawing no. Revision
A00.003 A

OLD SOUTH HEAD ROAD
STREET ELEVATION

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671- 683 OSH RD VAUCLUSE

A00
EXTERNAL PERSPECTIVE 04

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Drawing no.	Revision

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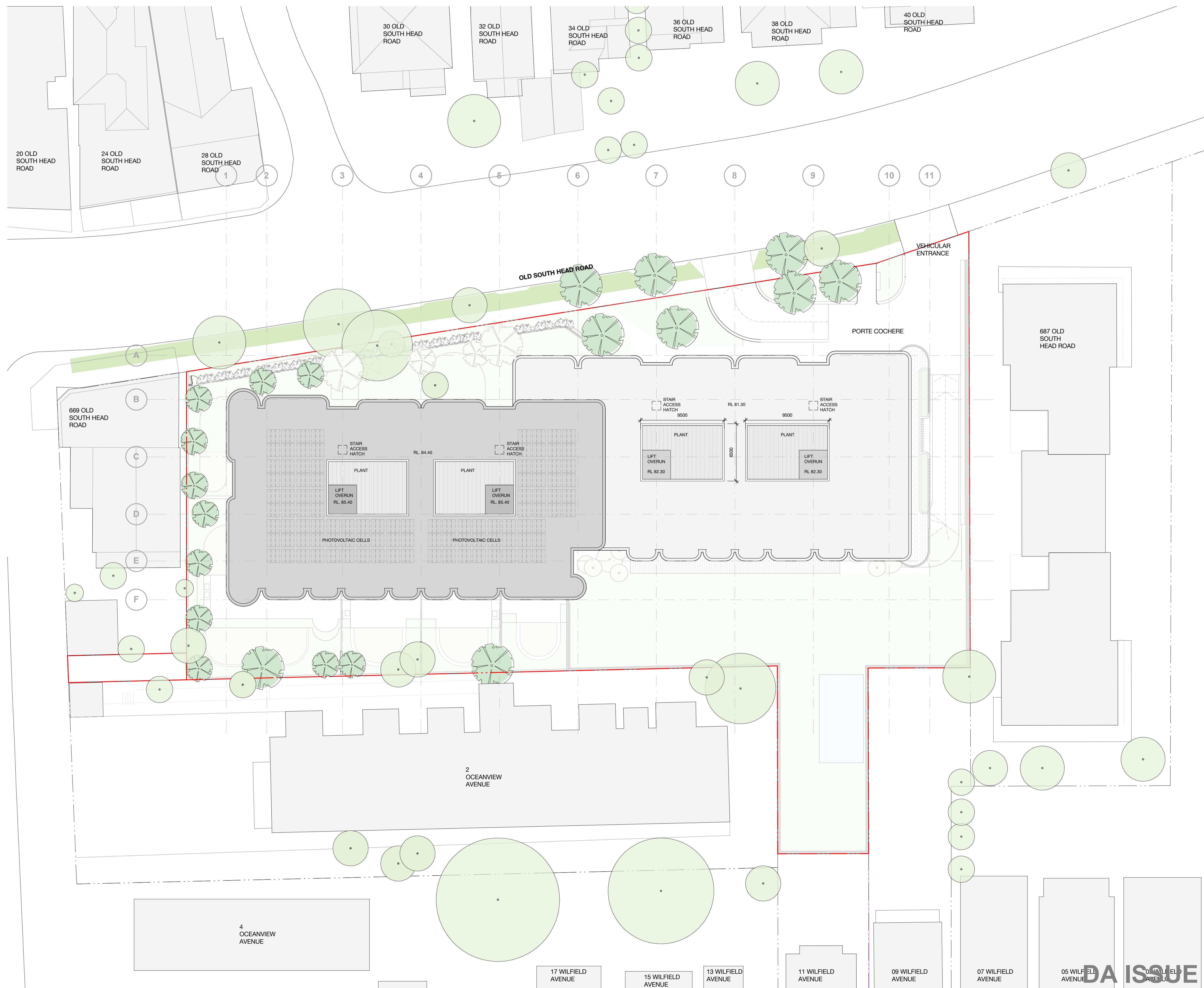
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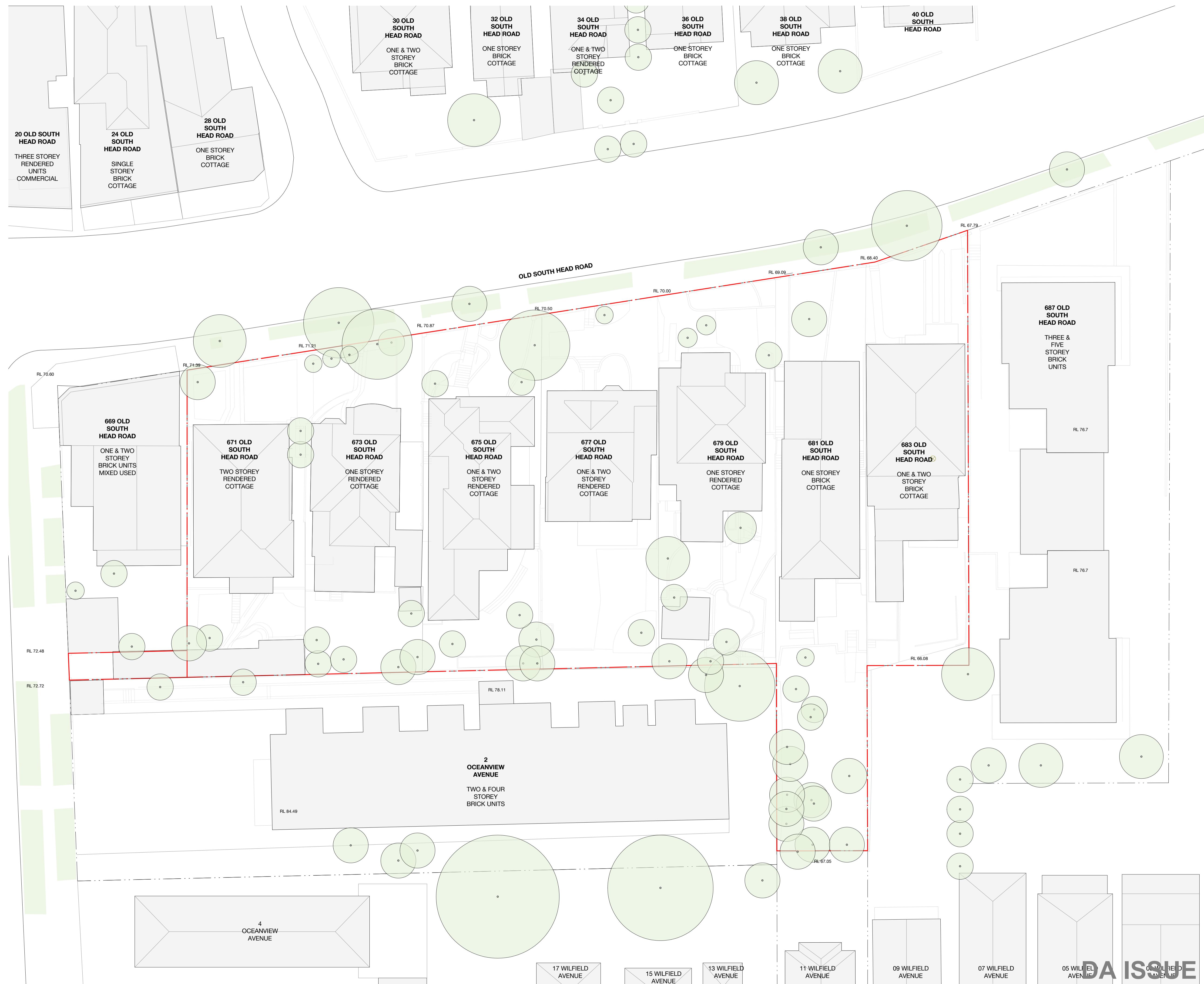
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1	21.09.23 ISSUE FOR INFORMATION	Initial
Rev	Date	Checked

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671-683 OSH RD VAUCLUSE

A01 EXISTING CONDITIONS

Status CONCEPT
Scale 1 : 200 @ A1
Drawn SH Checked
Project No. S12551
Plot Date 8/10/2021 12:31:19 AM
BIM
Drawing no. Revision

A01.002 A

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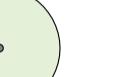
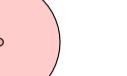
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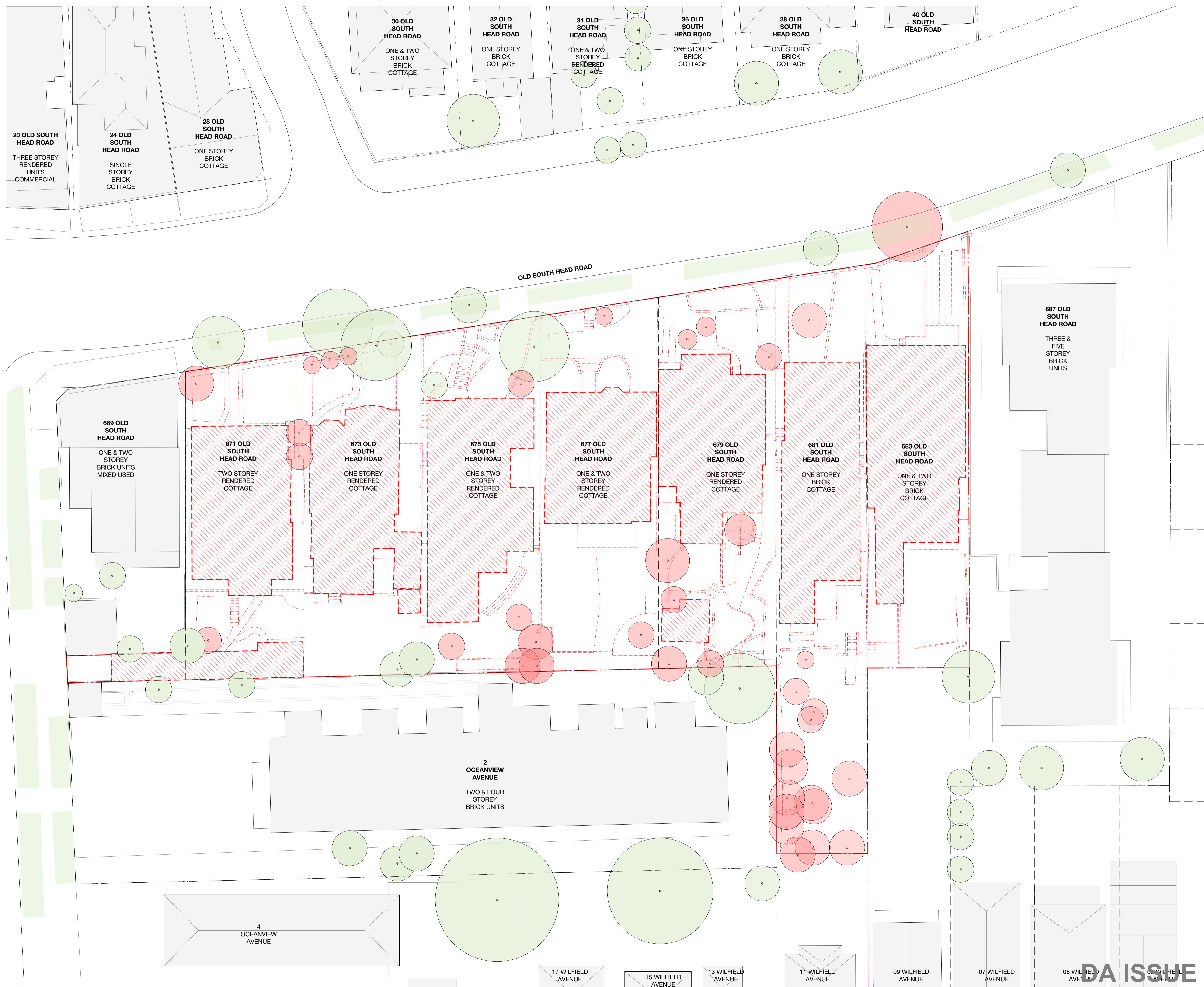
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Legend - Demolition Plan

-  EXISTING TREES
-  TREES TO BE REMOVED OR REPLANTED
-  TO BE DEMOLISHED



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Rev 1 Date 21.09.23 ISSUE FOR INFORMATION
SH Description Initial Checked

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A01
DEMOLITION



Status	CONCEPT
Scale	As indicated @ A1
Drawn	SH Checked
Project No.	S12551
Plot Date	8/10/2021 12:31:31 AM
BIM	

Drawing no. A01.003 Revision A

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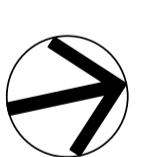
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21.09.23	ISSUE FOR INFORMATION	SH
21.09.09	ISSUE FOR INFORMATION	SH
21.09.01	ISSUE FOR INFORMATION	SH
Date	Description	Initial
		Checked

**VAUCLUSE SENIORS LIVING
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DA ISSUE BATES SMART





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VAUCLUSE SENIORS LIVING
671-683 OSH RD VAUCLUSE

A03
LEVEL 01 PLAN



Status	CONCEPT
Scale	1 : 200 @ A1
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Project No.	S12551
Pilot Date	8/10/2021 12:32:59 AM
BIM	
Drawing no.	Revision

A03.003

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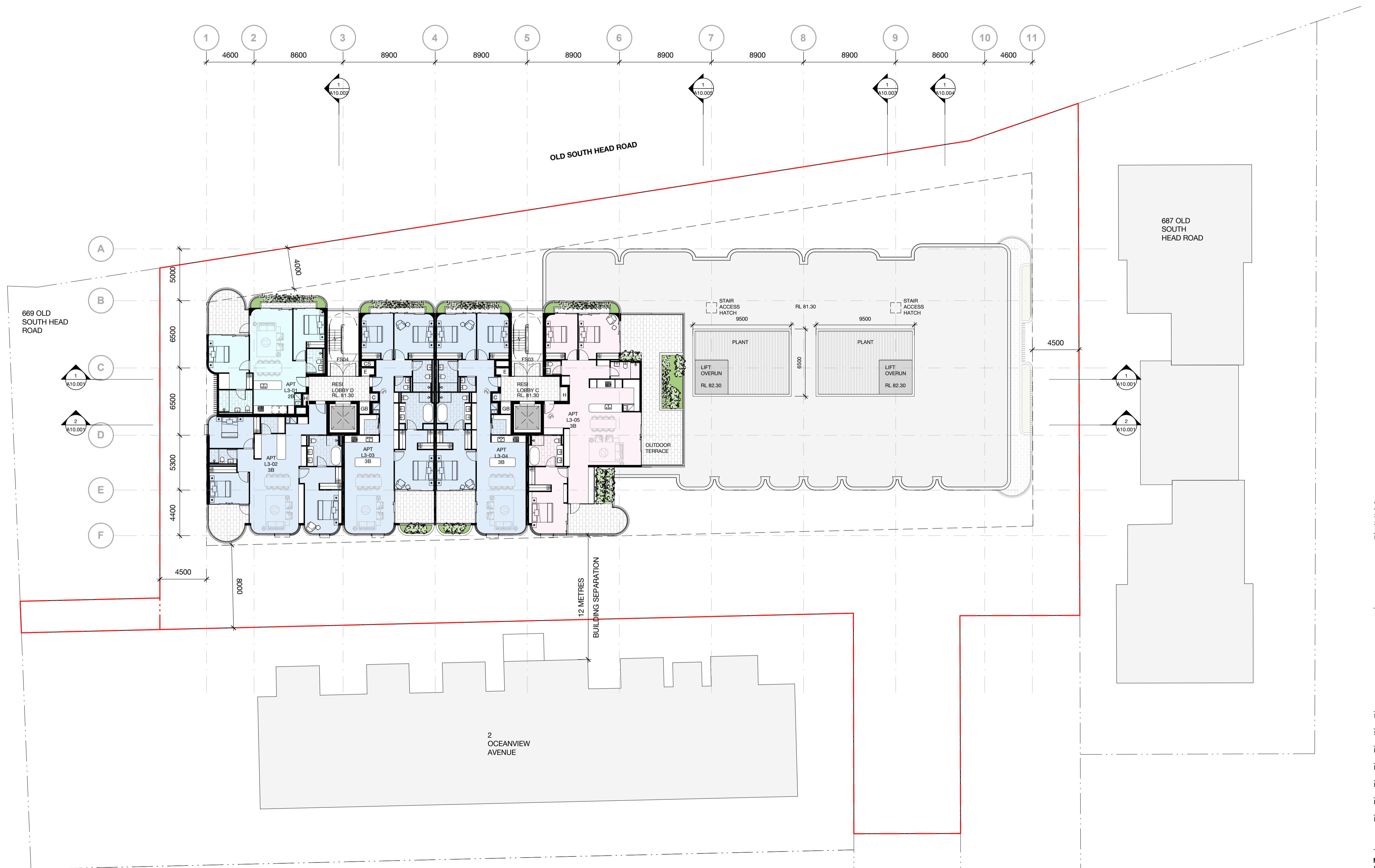
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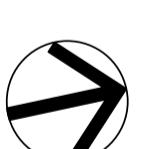




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**VAUCLUSE SENIORS LIVING
671-683 OSH RD VAUCLUSE**

**A03
LEVEL 03 PLAN**



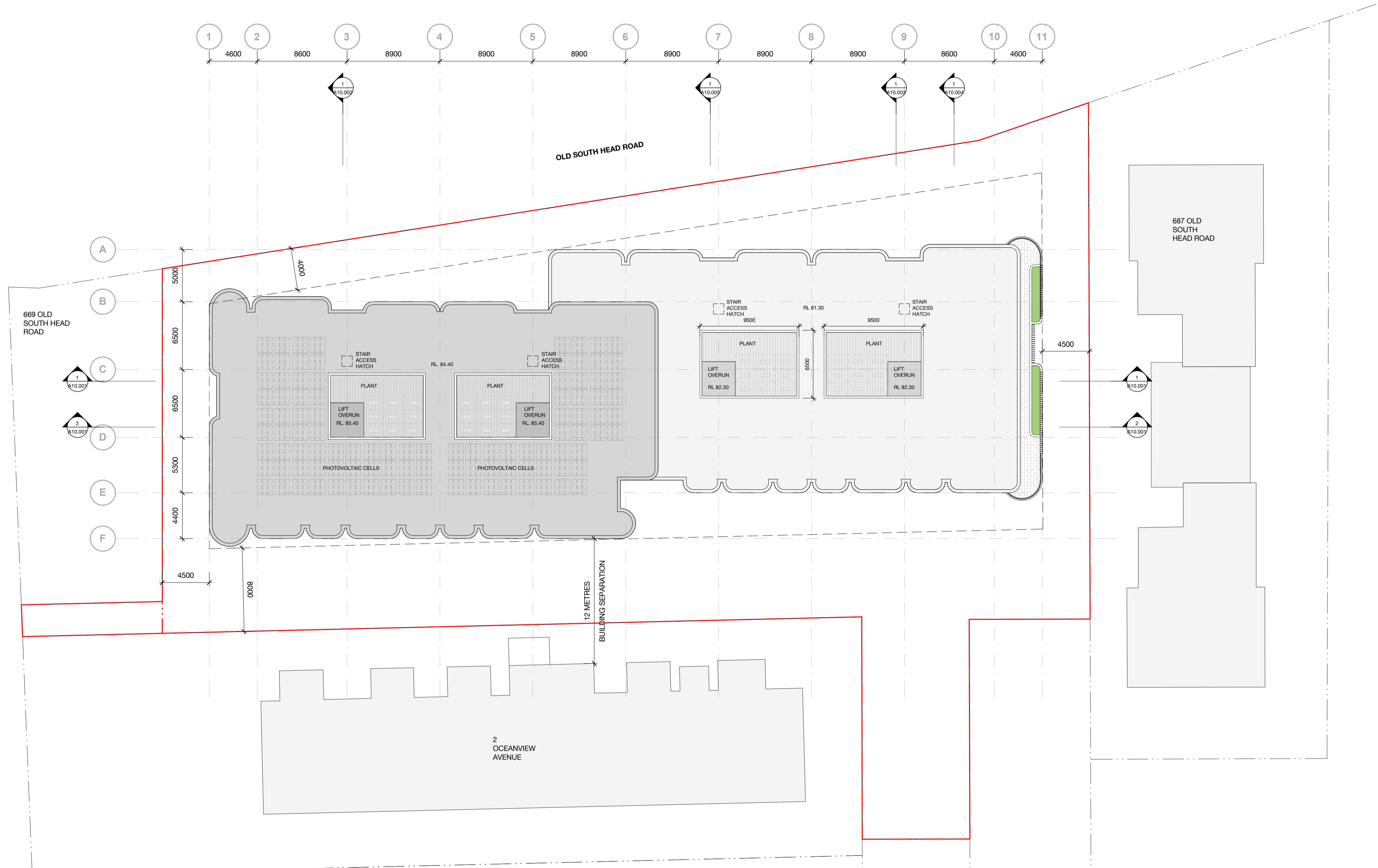
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BIM	
Drawing no.	Revision

A03.005 A

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A03 ROOF PLAN



Status	CONCEPT		
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BIM			

A03.006 **A**

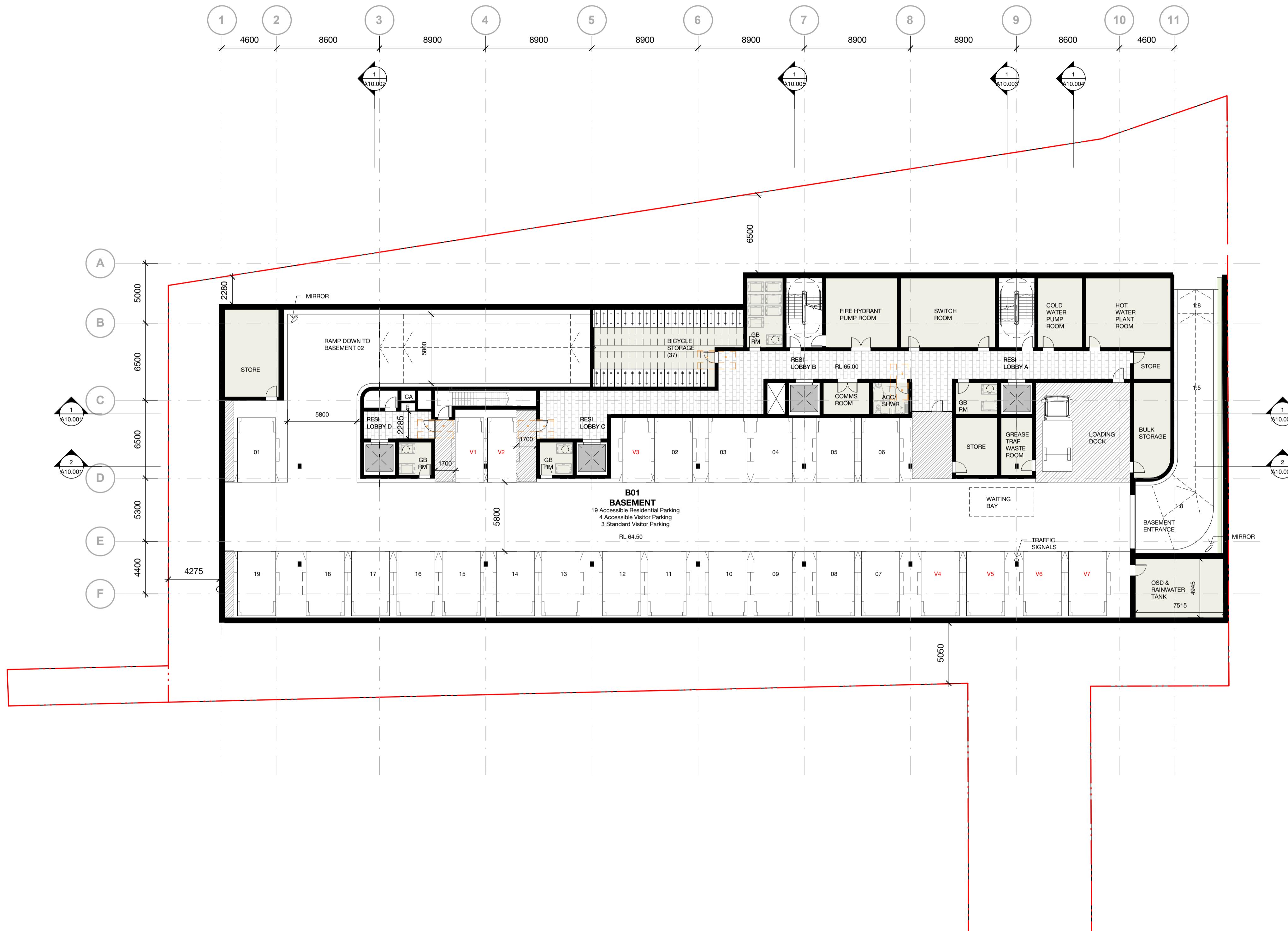
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A03
BASEMENT 01



Status	CONCEPT
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Drawing no.	Revision

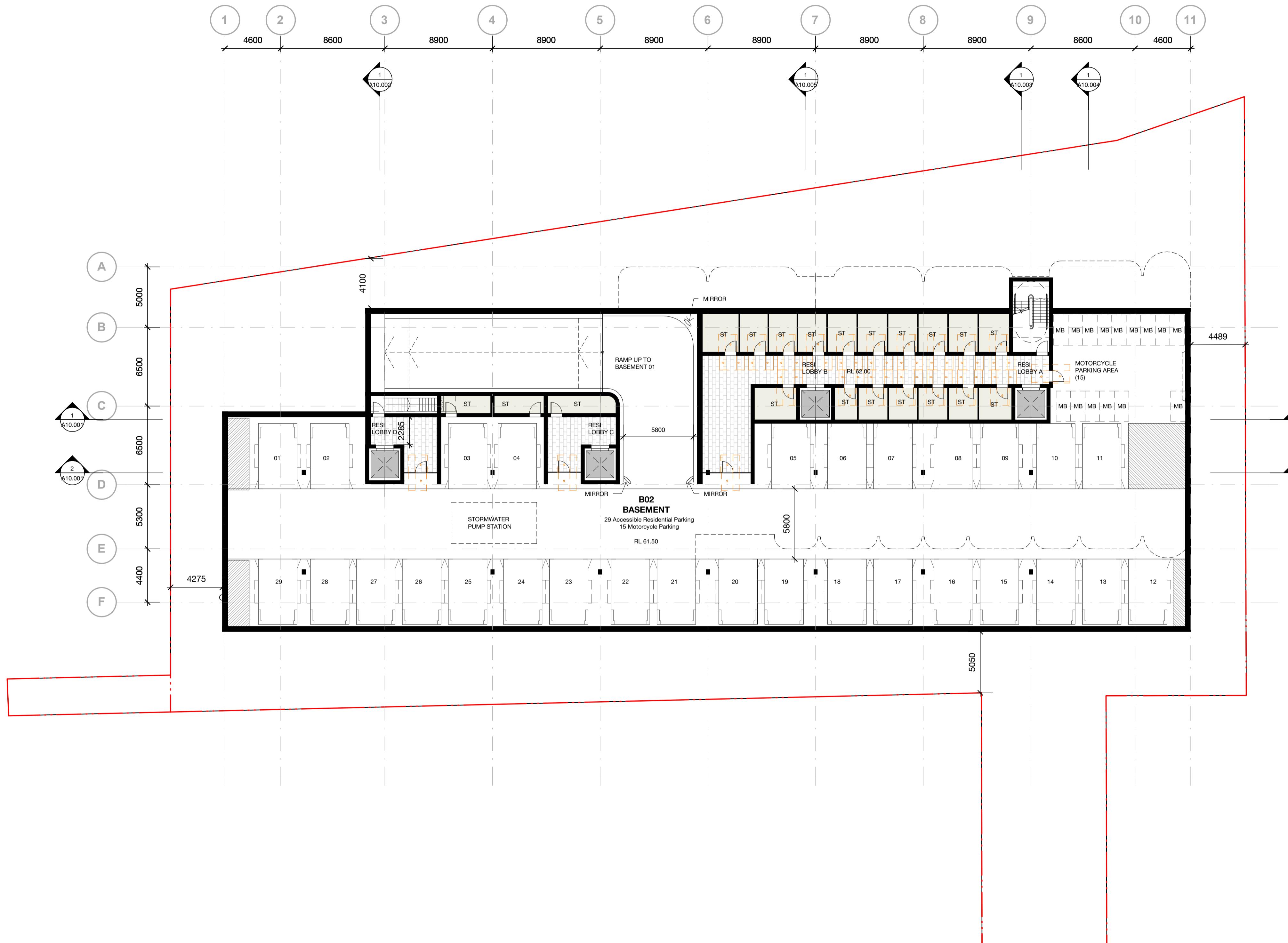
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A03
BASEMENT 02



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Drawing no.	Revision

A03.008

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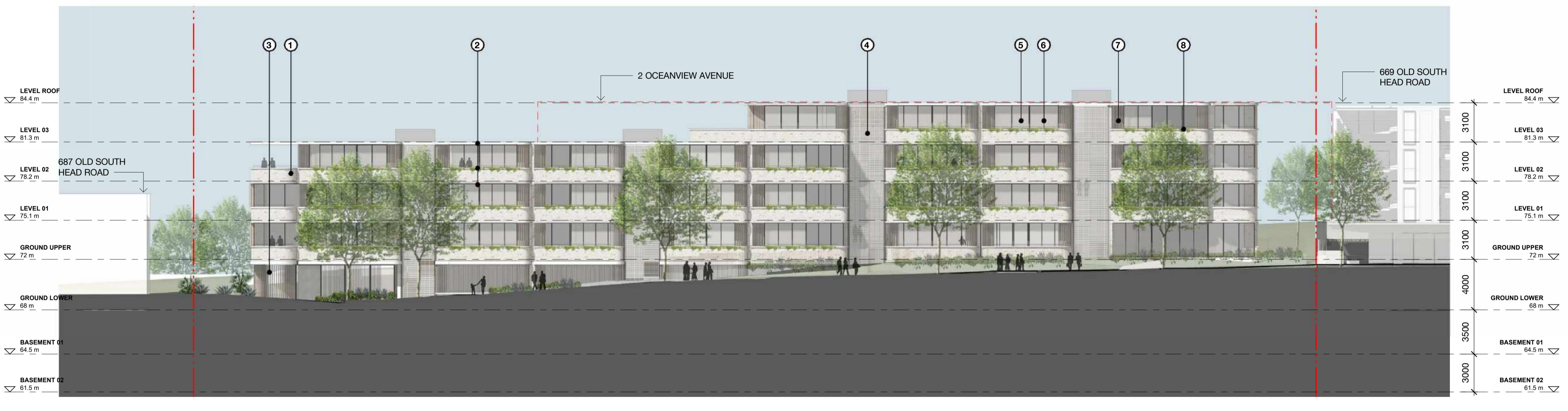
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Legend

- ① BRICK
- ② CONCRETE SLAB
- ③ TERRACOTTA SCREEN
- ④ GLASS BRICKS
- ⑤ GLASS - FIXED, AWNING WINDOWS AND SLIDING DOORS
- ⑥ METAL 01 - GLAZING FRAMES
- ⑦ METAL 02 - BALUSTRADE HANDRAILS
- ⑧ LANDSCAPE PLANTING



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A09
BUILDING ELEVATION

Status	CONCEPT
Scale	As indicated @ A1
Drawn	SH Checked -
Project No.	S12551
Plot Date	8/10/2021 12:34:06 AM
BIM	
Drawing no.	
Revision	

A09.001

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2 WEST ELEVATION

1:200

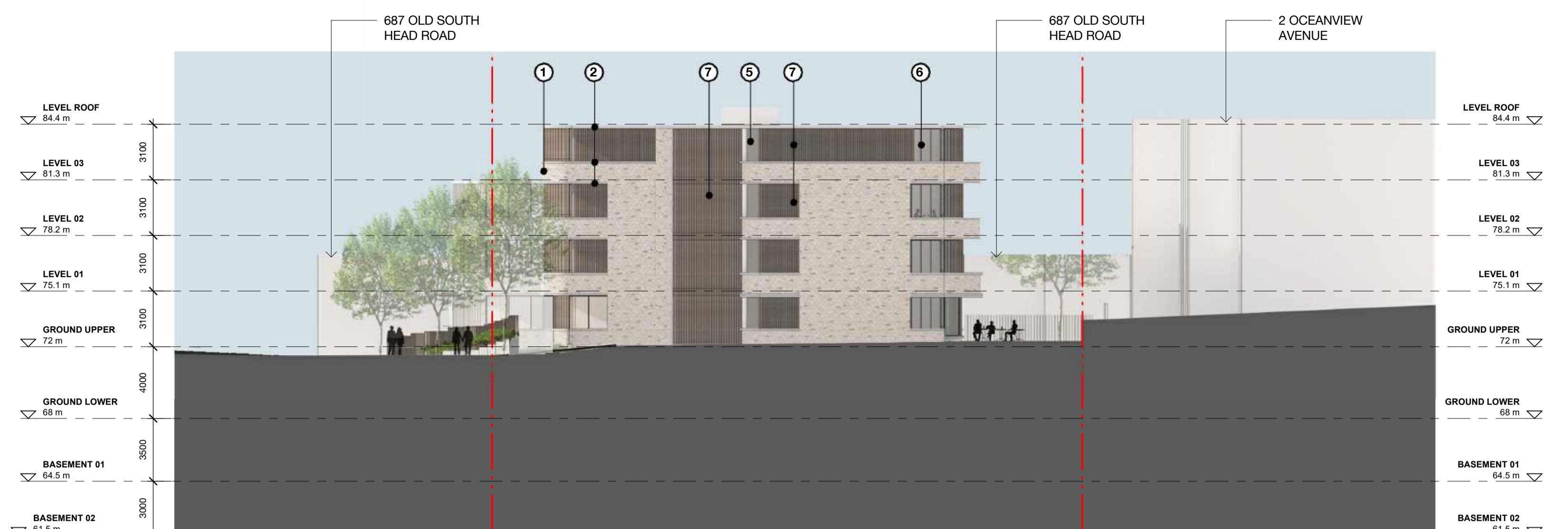
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Legend

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- ④ GLASS BRICKS
- ⑤ GLASS - FIXED, AWNING WINDOWS AND SLIDING DOORS
- ⑥ METAL 01 - GLAZING FRAMES
- ⑦ METAL 02 - BALUSTRADE HANDRAILS
- ⑧ LANDSCAPE PLANTING



1 SOUTH ELEVATION

1:200

A 21.10.07 DEVELOPMENT APPLICATION
2 21.10.01 ISSUE FOR INFORMATION
1 21.09.23 ISSUE FOR INFORMATION
Rev Date Description SH SH SH Checked

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VAUCLUSE SENIORS LIVING
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A09
BUILDING ELEVATION

Status	CONCEPT
Scale	As indicated @ A1
Drawn	SH Checked
Project No.	S12551
Plot Date	8/10/2021 12:34:22 AM
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Drawing no. Revision

A09.002 A

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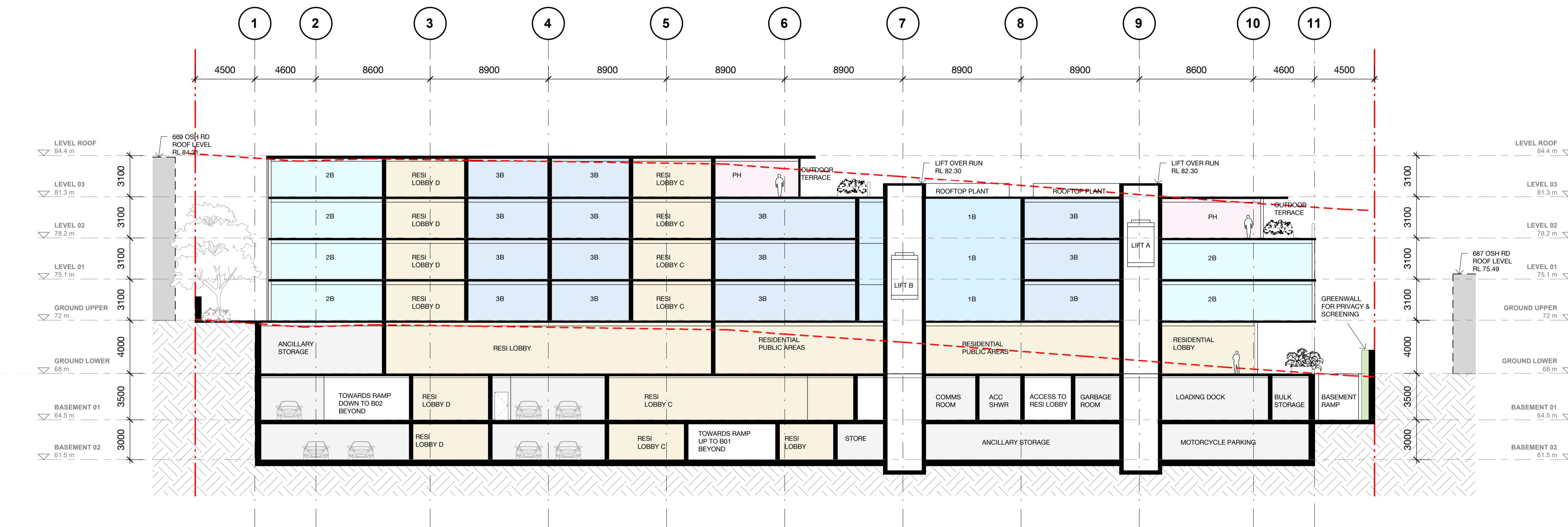
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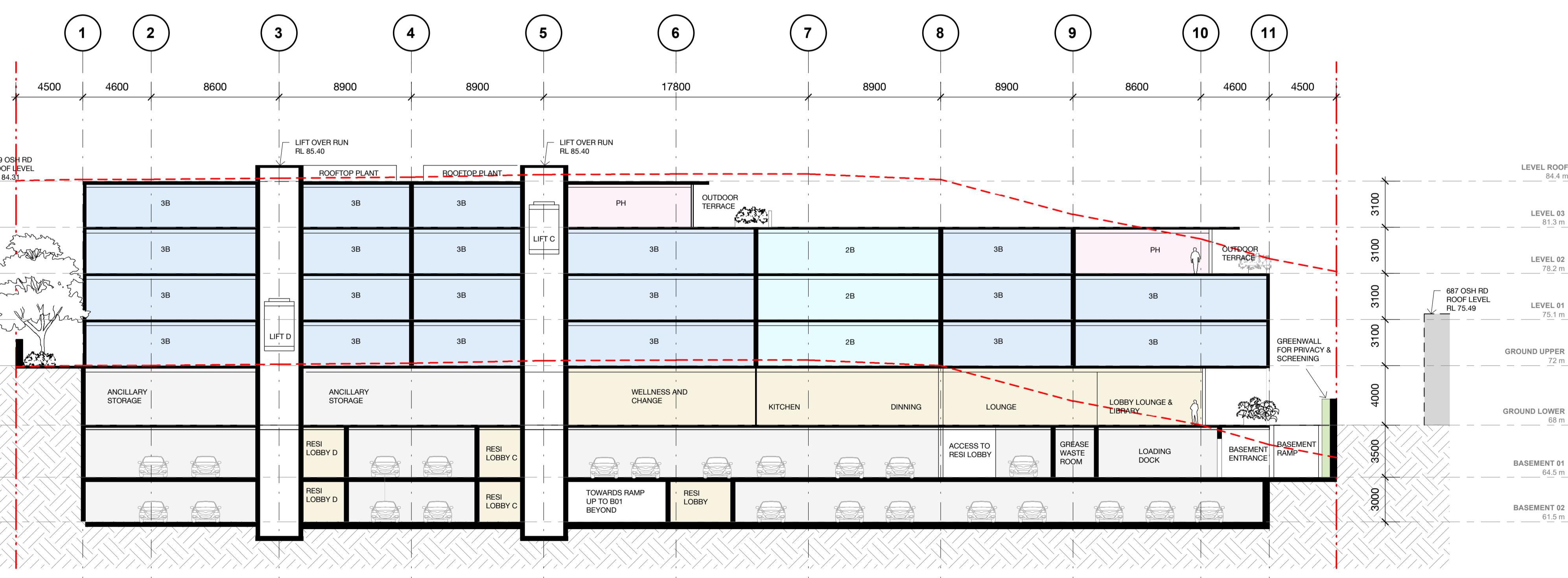
2 EAST ELEVATION

1:200

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SECTION 01



SECTION 02

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3	21.10.01 ISSUE FOR INFORMATION	SH
2	21.09.23 ISSUE FOR INFORMATION	SH
1	21.09.01 ISSUE FOR INFORMATION	SH

Rev Date Description Initial Checked

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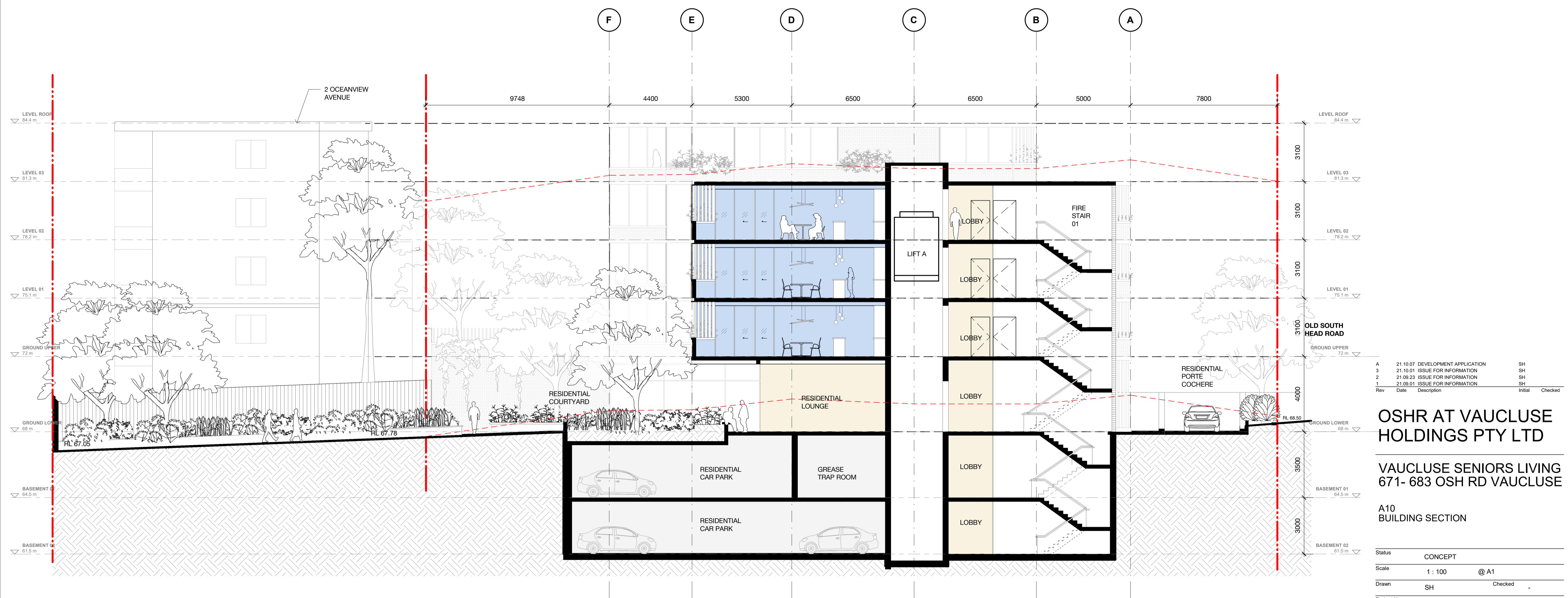
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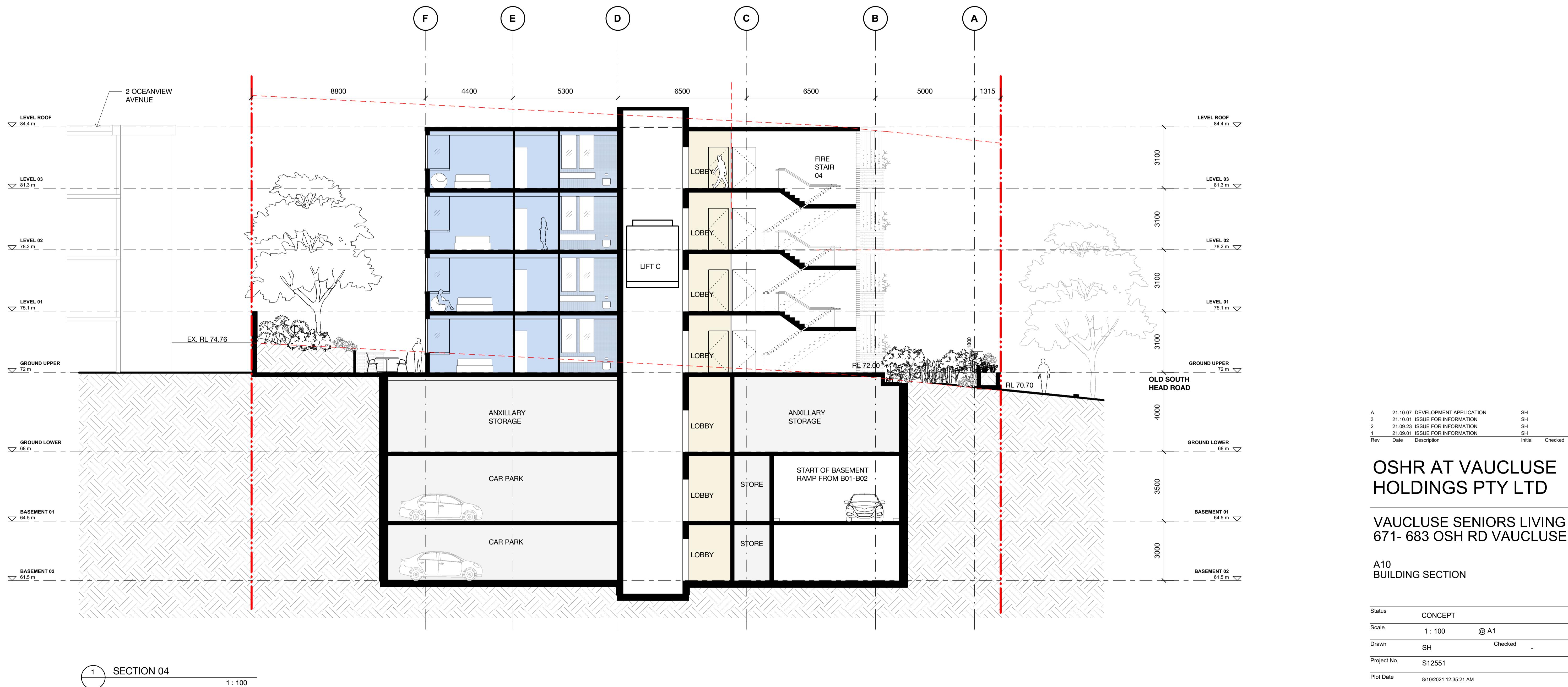
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Drawing no.	
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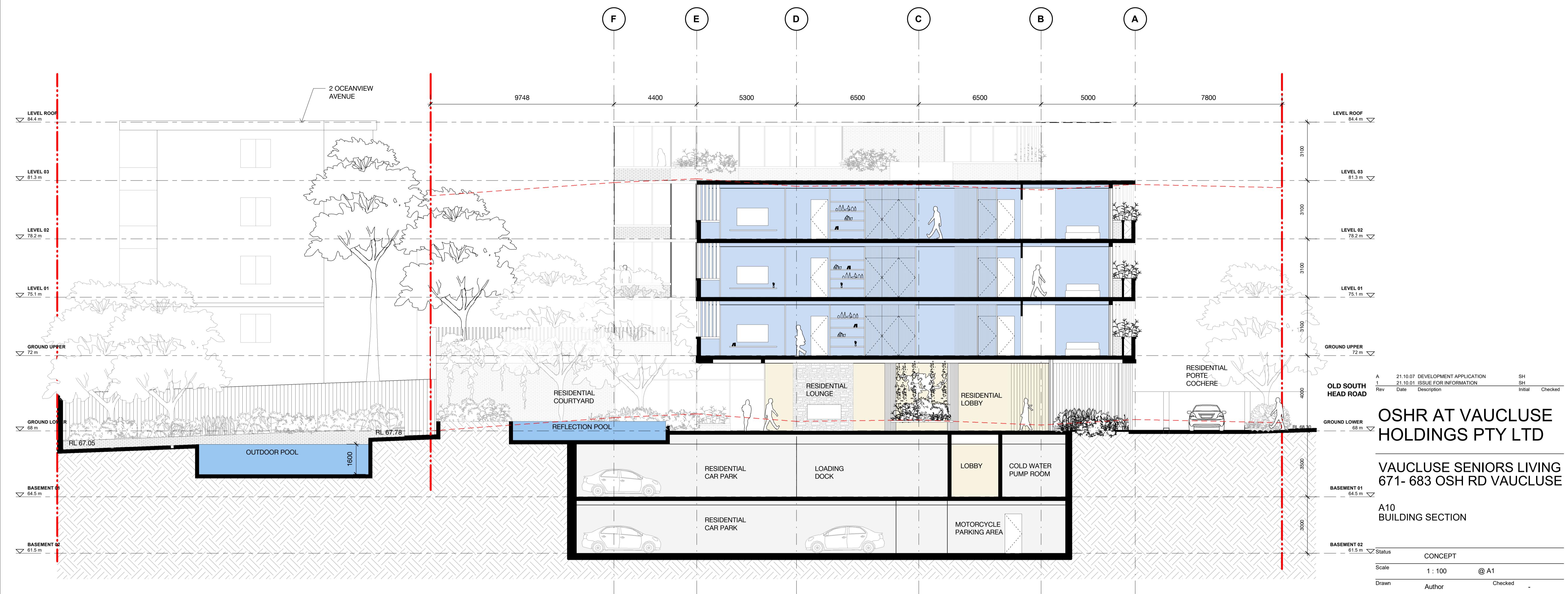


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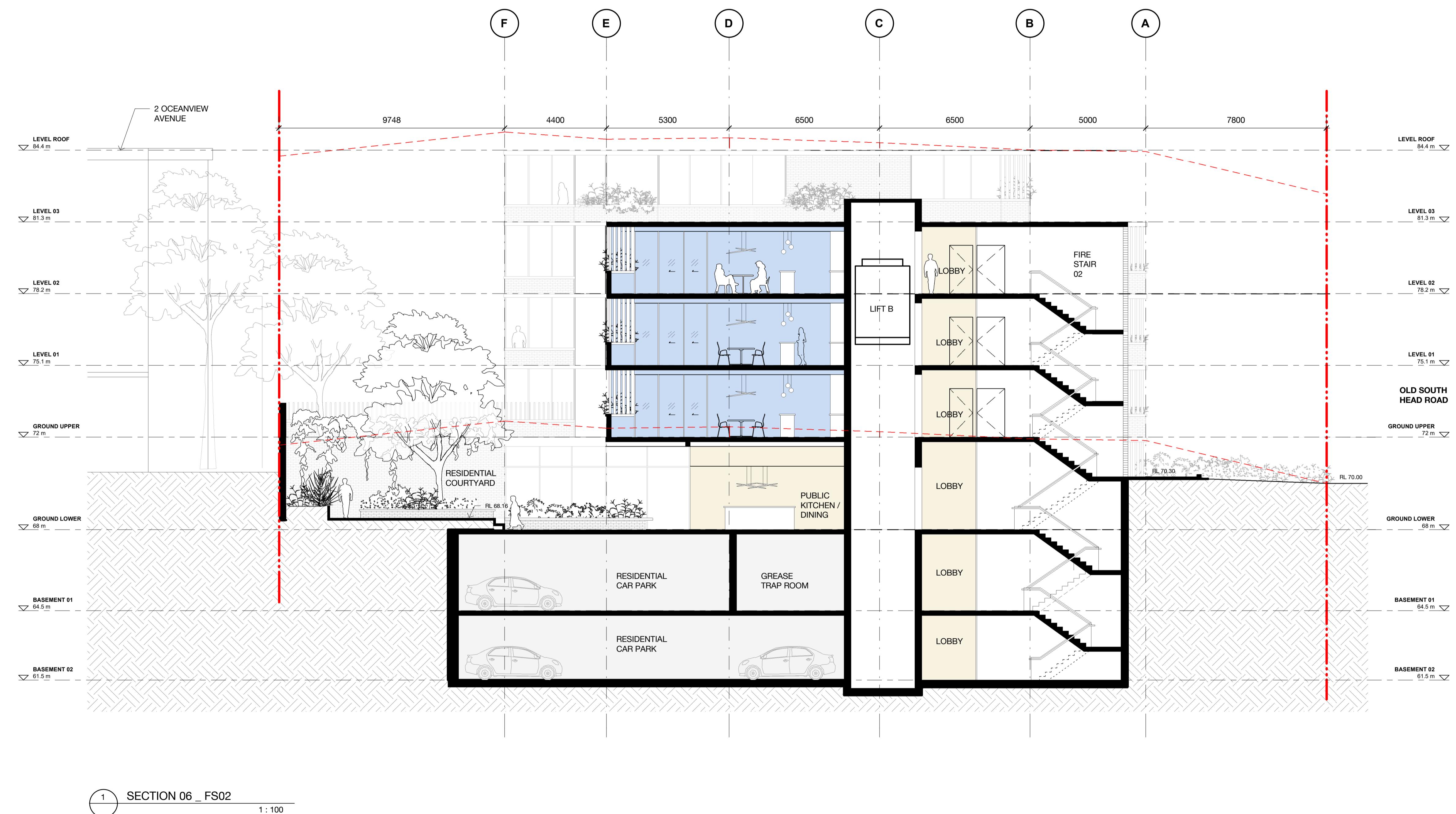


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A10 BUILDING SECTION

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Drawing no. Revision

A10.005 **A**

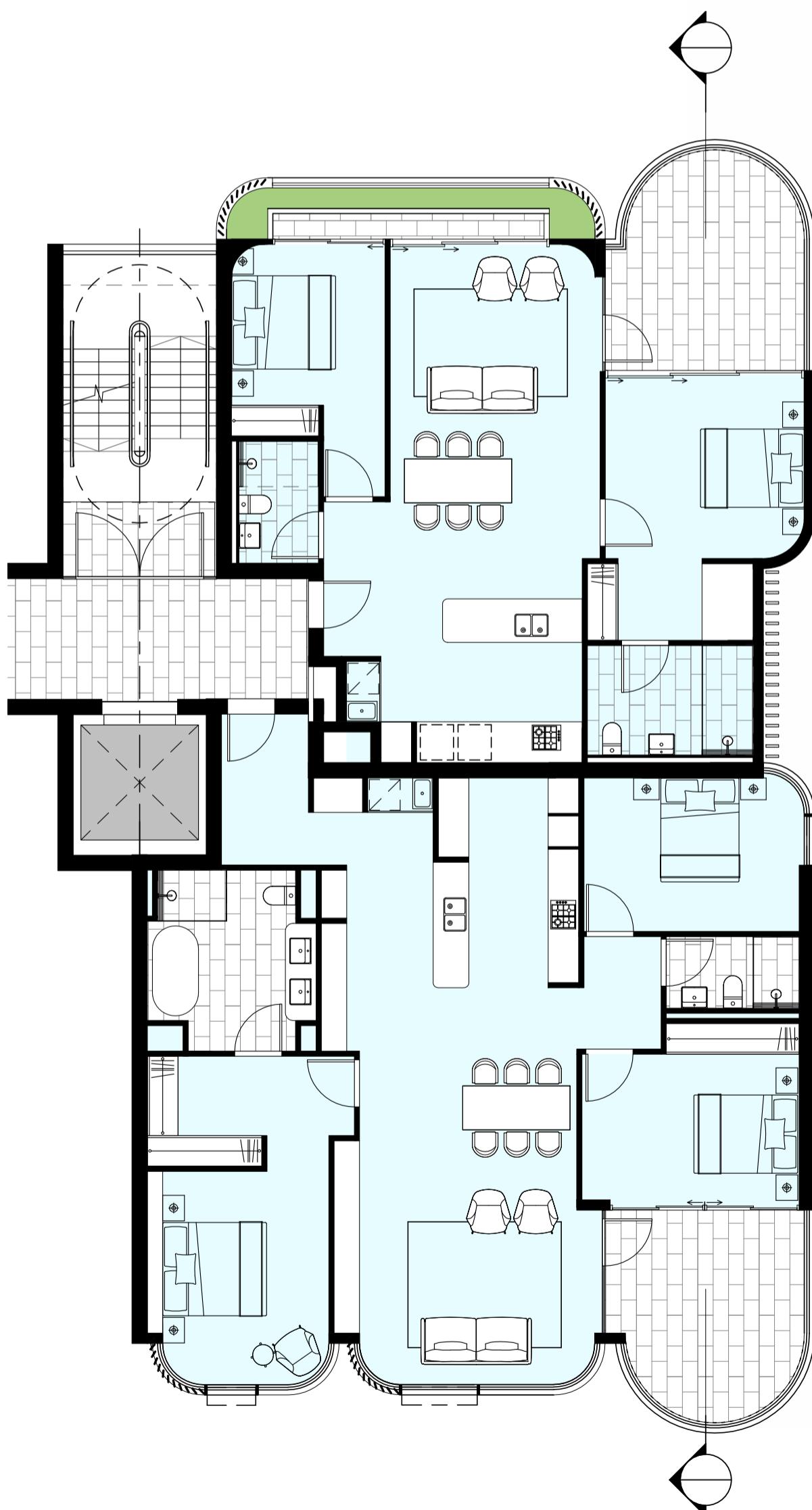
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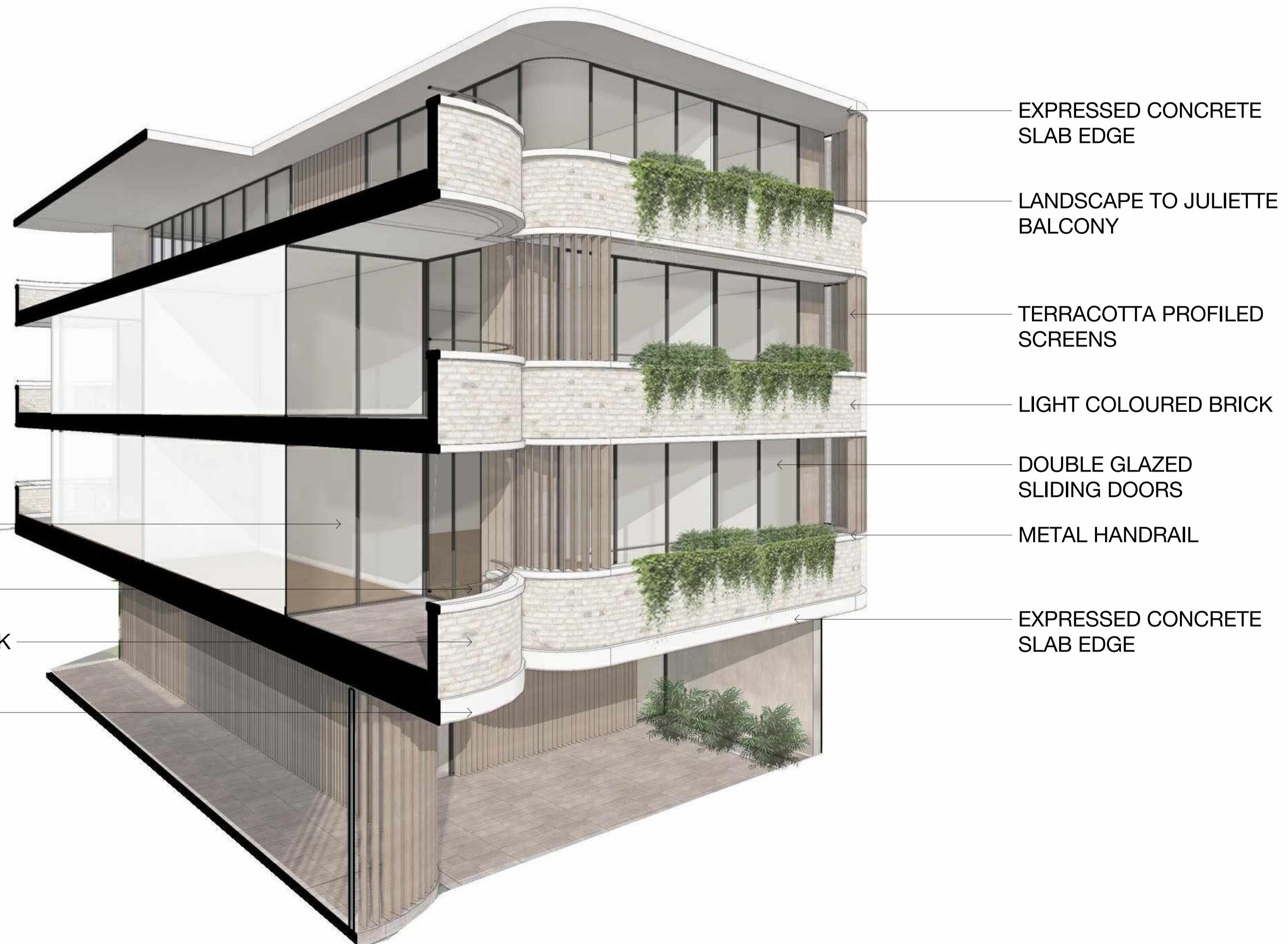
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EXTERIOR PERSPECTIVE



KEY PLAN



SECTIONAL AXO OF FACADE TYPE 01

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- ④ GLASS BRICKS
- ⑤ GLASS – FIXED, AWNING WINDOWS AND SLIDING DOORS
- ⑥ METAL 01 - GLAZING FRAMES
- ⑦ METAL 02 - BALUSTRADE HANDRAILS
- ⑧ LANDSCAPE PLANTING

A 21.10.07 DEVELOPMENT APPLICATION
Rev Date Description SH Initial Checked
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A11
FAÇADE TYPE 01

Status	CONCEPT
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Drawing no.	Revision

A11.001 A

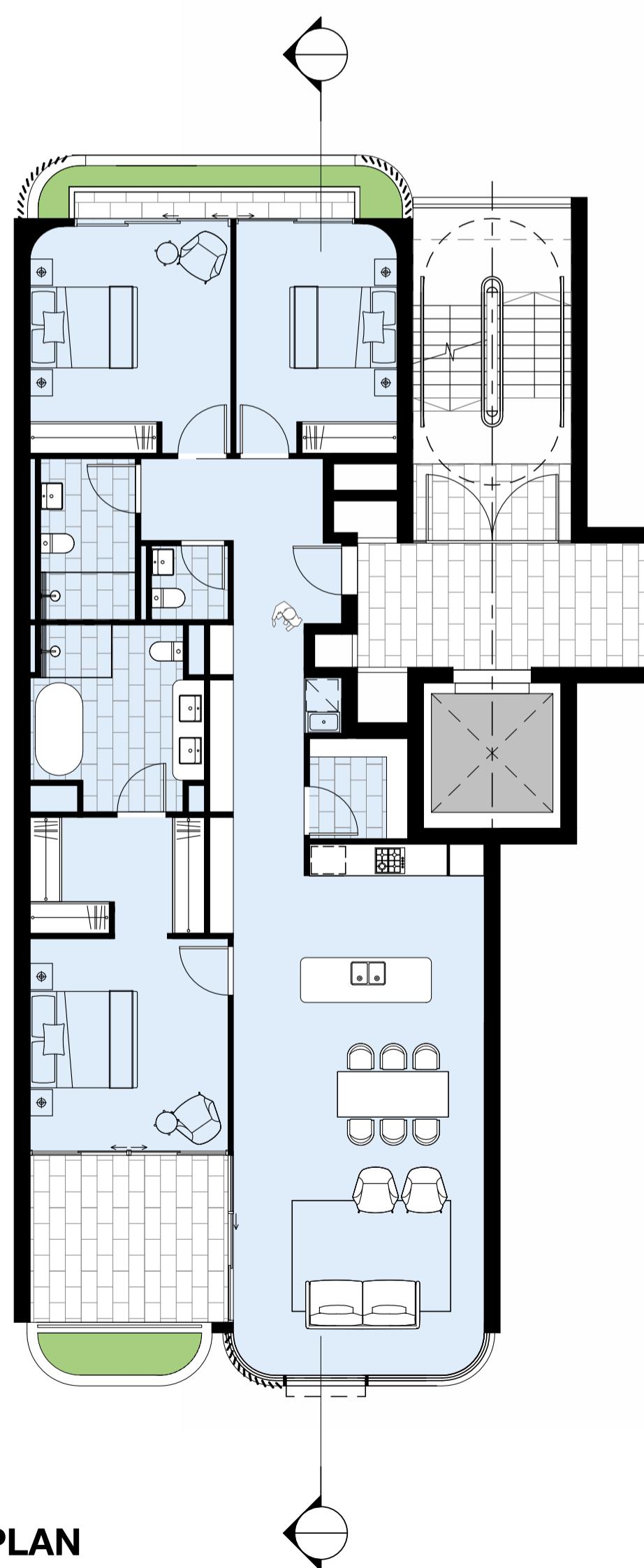
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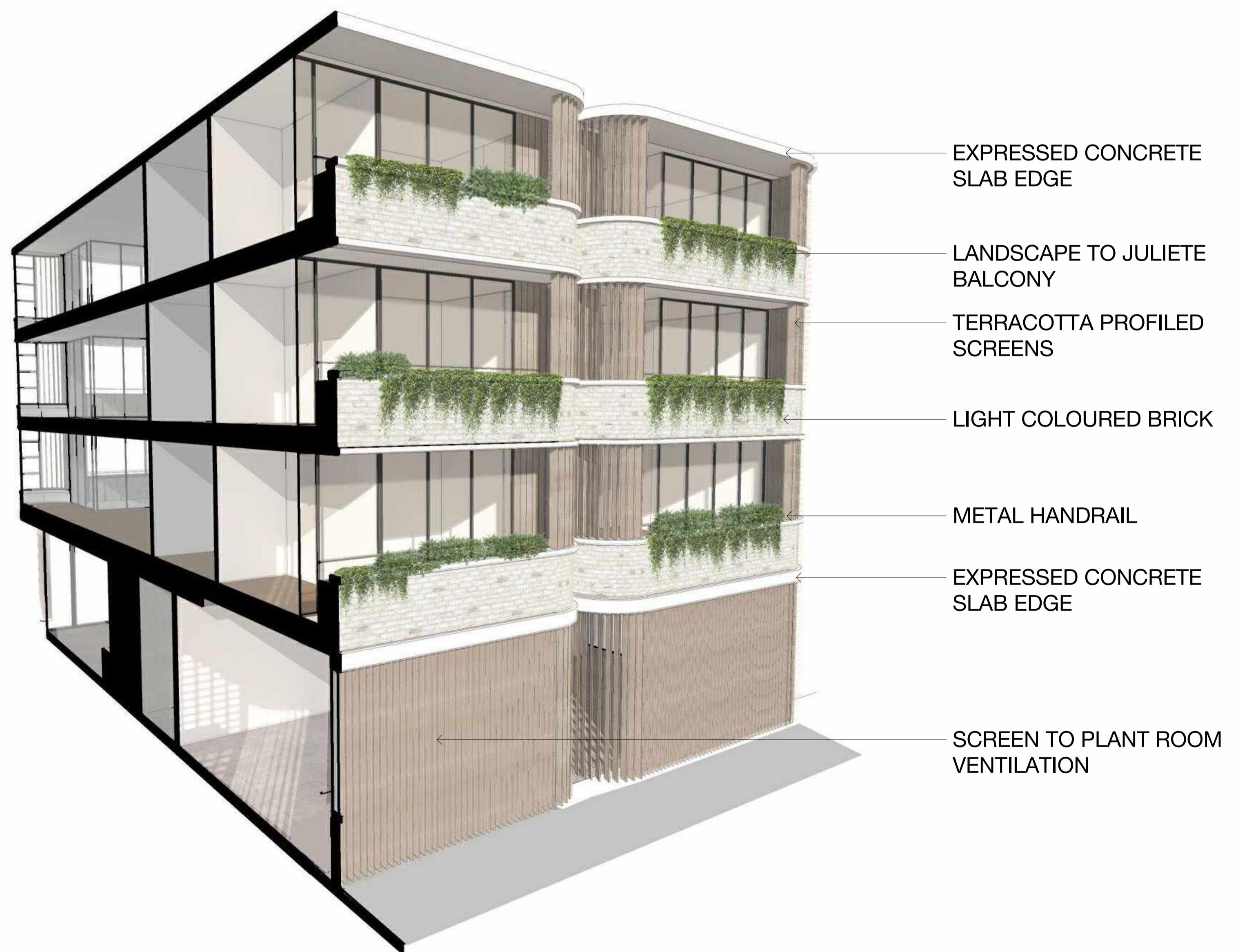
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EXTERIOR PERSPECTIVE



KEY PLAN



SECTIONAL AXO OF FACADE TYPE 02

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- ⑥ METAL 01 - GLAZING FRAMES
- ⑦ METAL 02 - BALUSTRADE HANDRAILS
- ⑧ LANDSCAPE PLANTING

A 21.10.07 DEVELOPMENT APPLICATION SH Initial Checked

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A11
FAÇADE TYPE 02

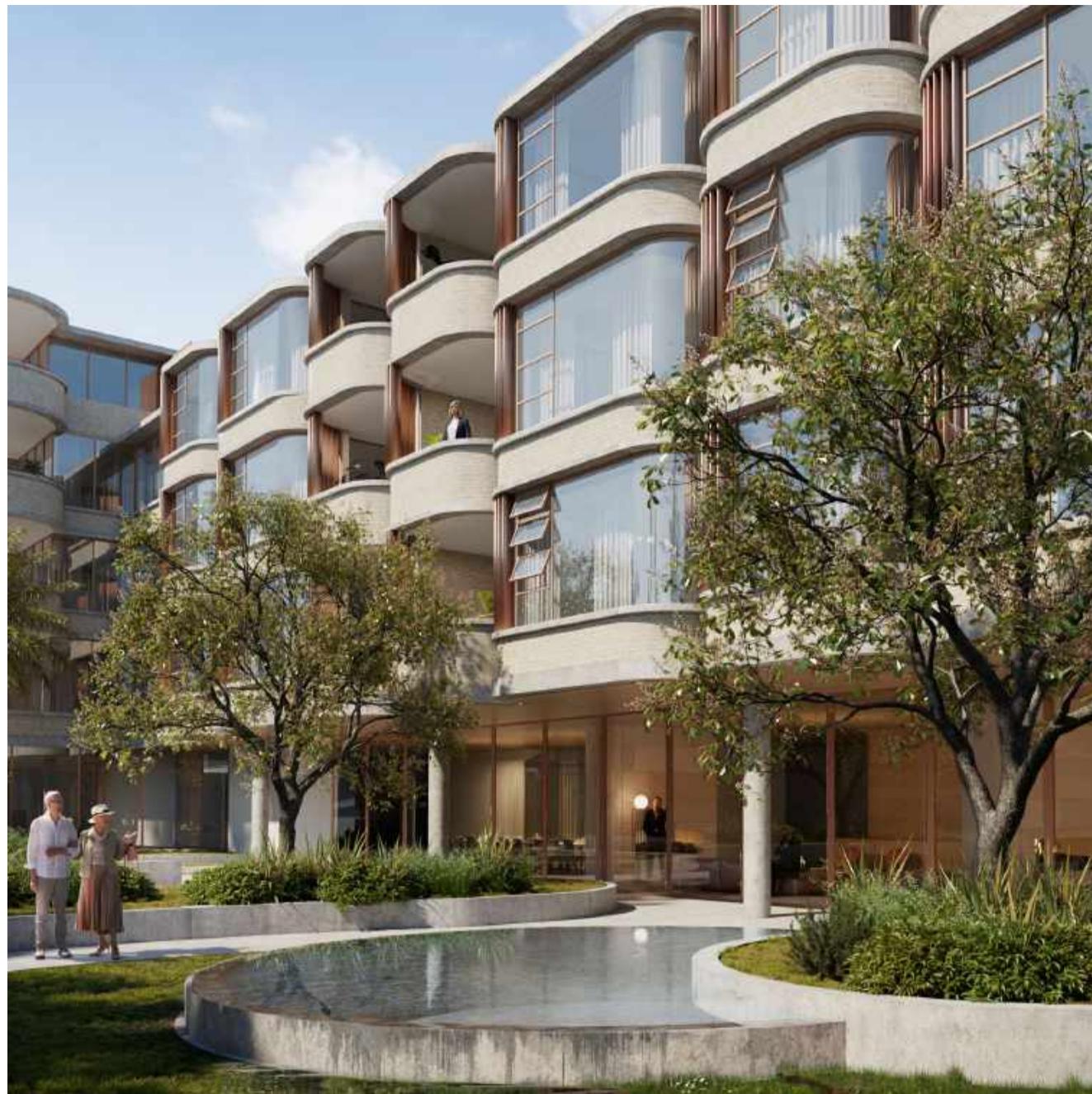
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A11.002 A

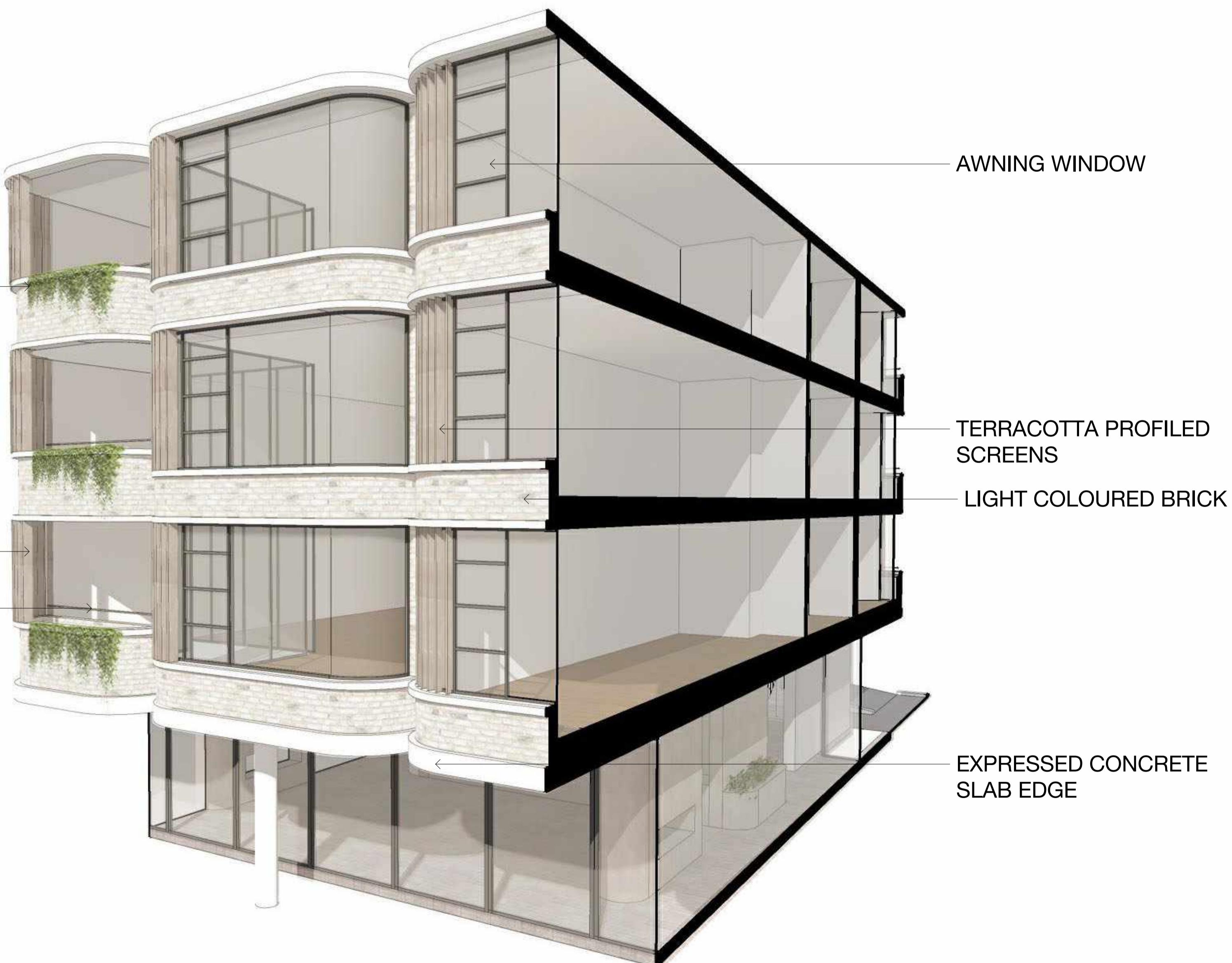
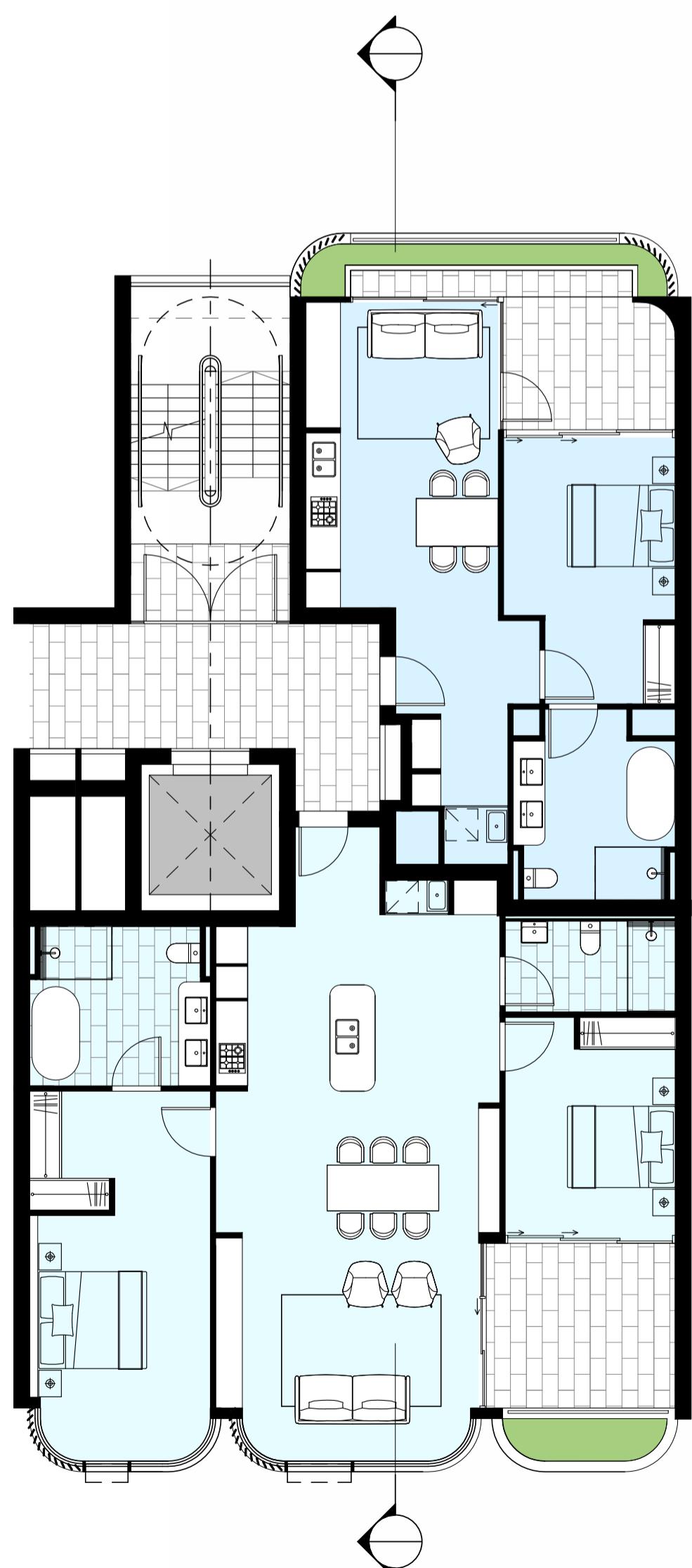
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EXTERIOR PERSPECTIVE



KEY PLAN

SECTIONAL AXO OF FACADE TYPE 03

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- ⑤ GLASS – FIXED, AWNING WINDOWS AND SLIDING DOORS
- ⑥ METAL 01 - GLAZING FRAMES
- ⑦ METAL 02 - BALUSTRADE HANDRAILS
- ⑧ LANDSCAPE PLANTING

A 21.10.07 DEVELOPMENT APPLICATION
Rev Date Description SH Initial Checked

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A11
FAÇADE TYPE 03

Status	CONCEPT
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Plot Date	8/10/2021 12:36:12 AM
BIM	
Drawing no.	Revision

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A 21.10.07 DEVELOPMENT APPLICATION SH
 4 21.10.01 ISSUE FOR INFORMATION SH
 3 21.09.23 ISSUE FOR INFORMATION SH
 2 21.09.09 ISSUE FOR INFORMATION SH
 1 21.09.06 ISSUE FOR INFORMATION SH
 Rev Date Description Initial Checked

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A13
APARTMENT TYPE - 3B

Status	CONCEPT
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Drawn	SH Checked
Project No.	S12551
Plot Date	8/10/2021 12:36:30 AM
BIM	
Drawing no.	
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A13.001 **A**

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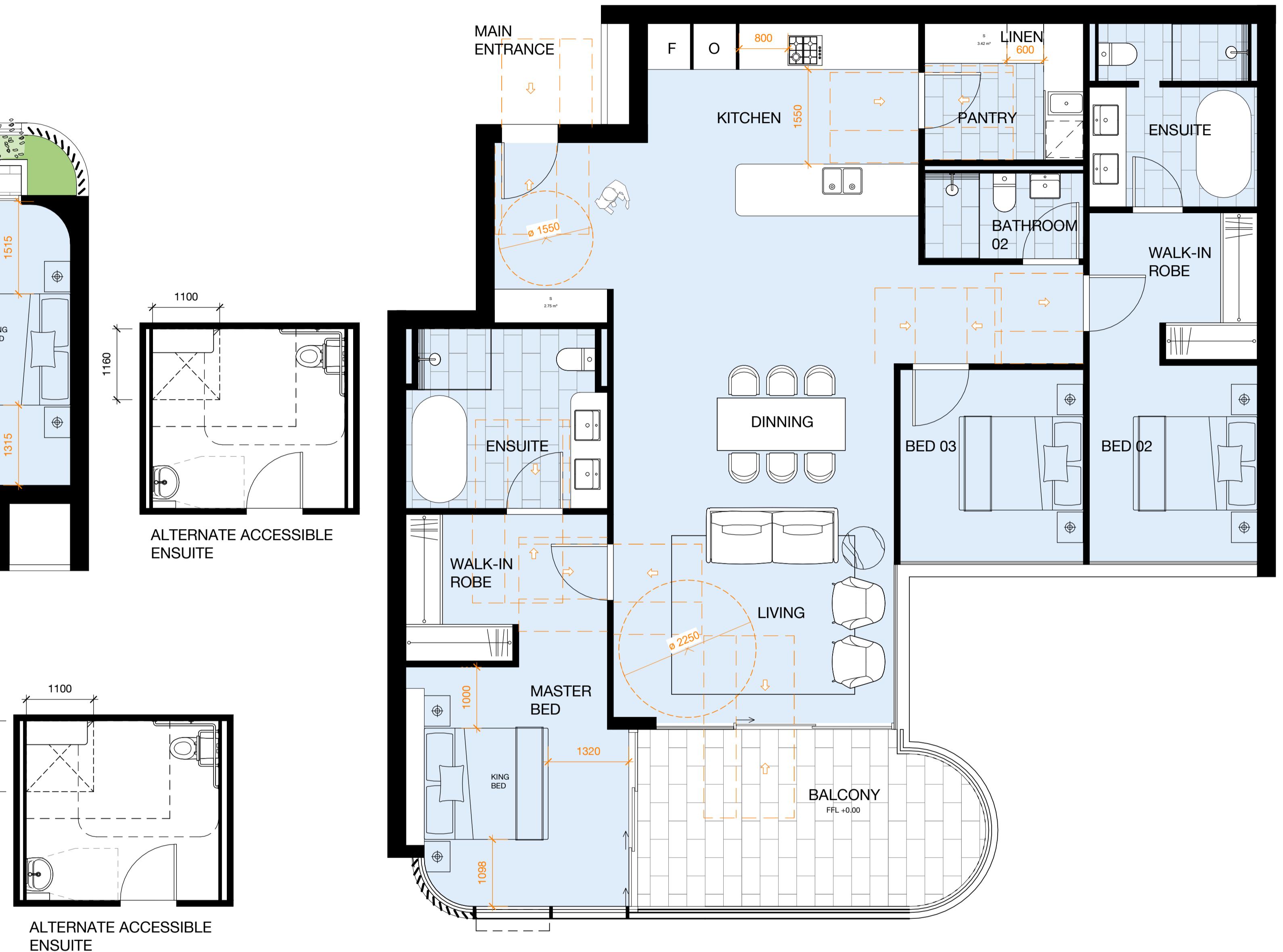
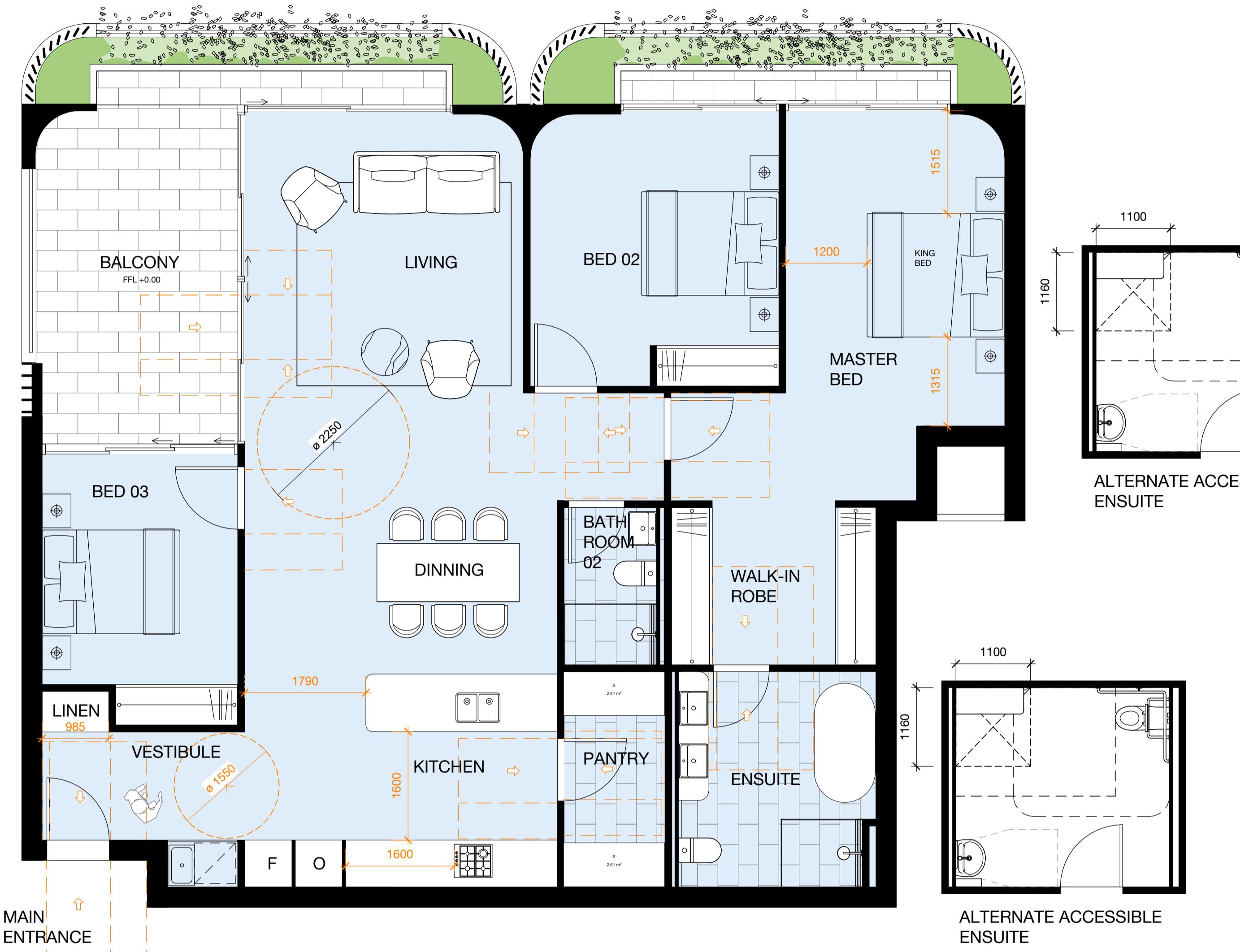
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Legend

AS 1428 & AS 4299 CIRCULATION & DISTANCE REQUIREMENTS

GENERAL NOTES

- CEILING FAN TO ALL LIVING ROOMS AND BEDROOMS



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A13
APARTMENT TYPE - 3B

Status	CONCEPT
Scale	As indicated @ A1
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Project No.	S12551
Plot Date	8/10/2021 12:42:57 AM
BIM	
Drawing no.	
Revision	

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VAUCLEUSE SENIORS LIVING
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A13
APARTMENT TYPE -3B

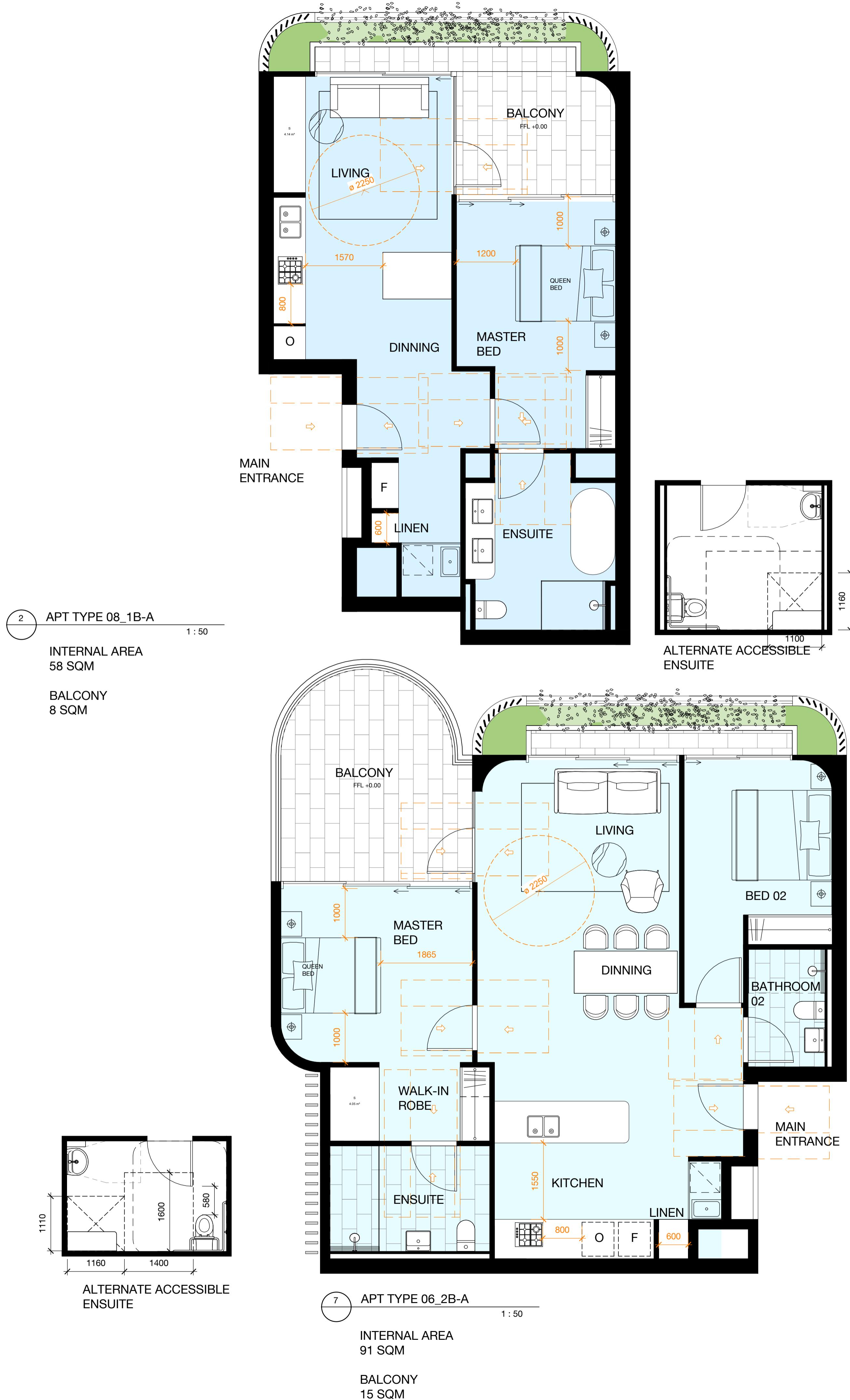
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APT TYPE 07, 08, R

INTERNAL AREA

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— — — AS 1428 & AS 4299 CIRCULATION & DISTANCE REQUIREMENTS

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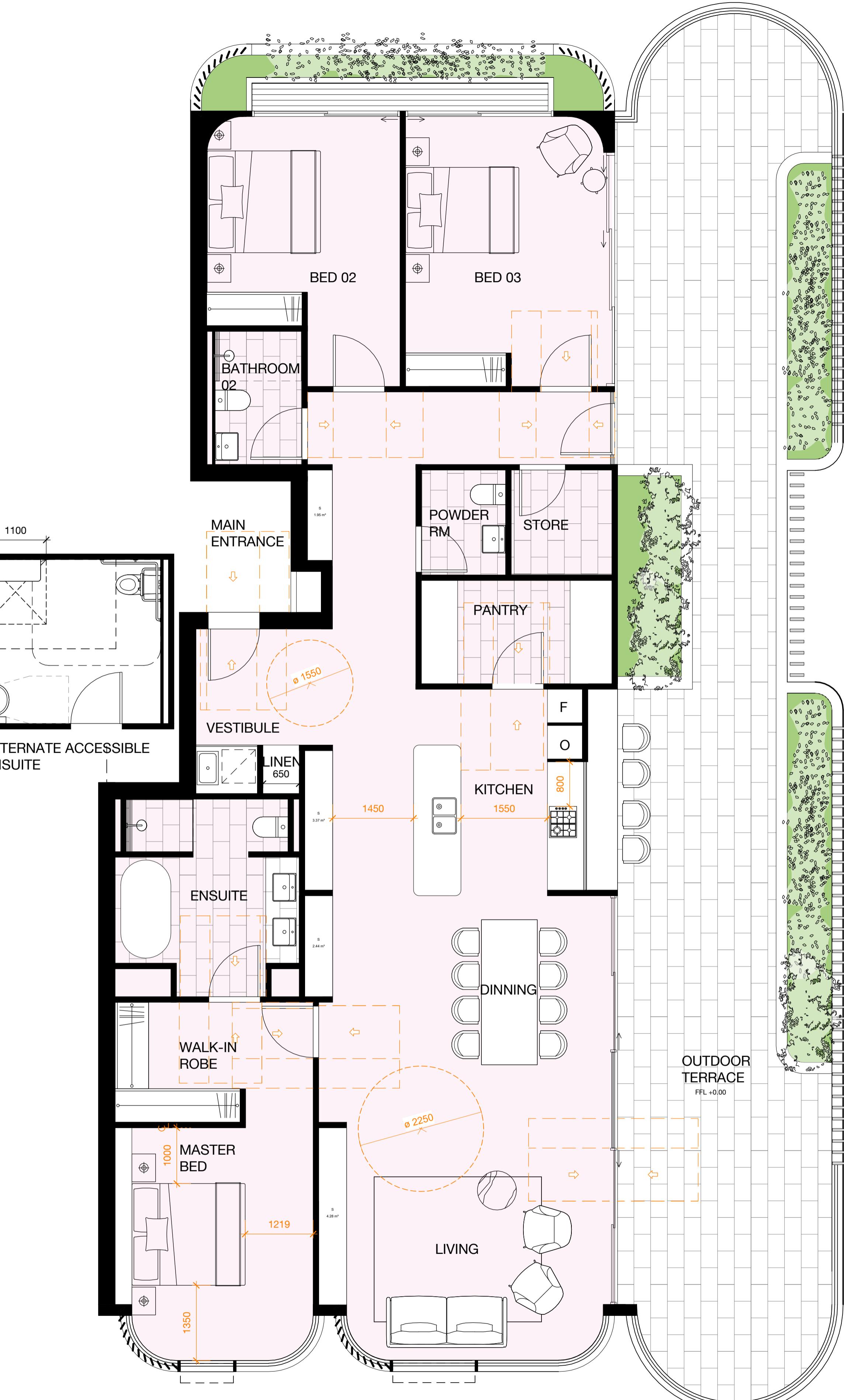
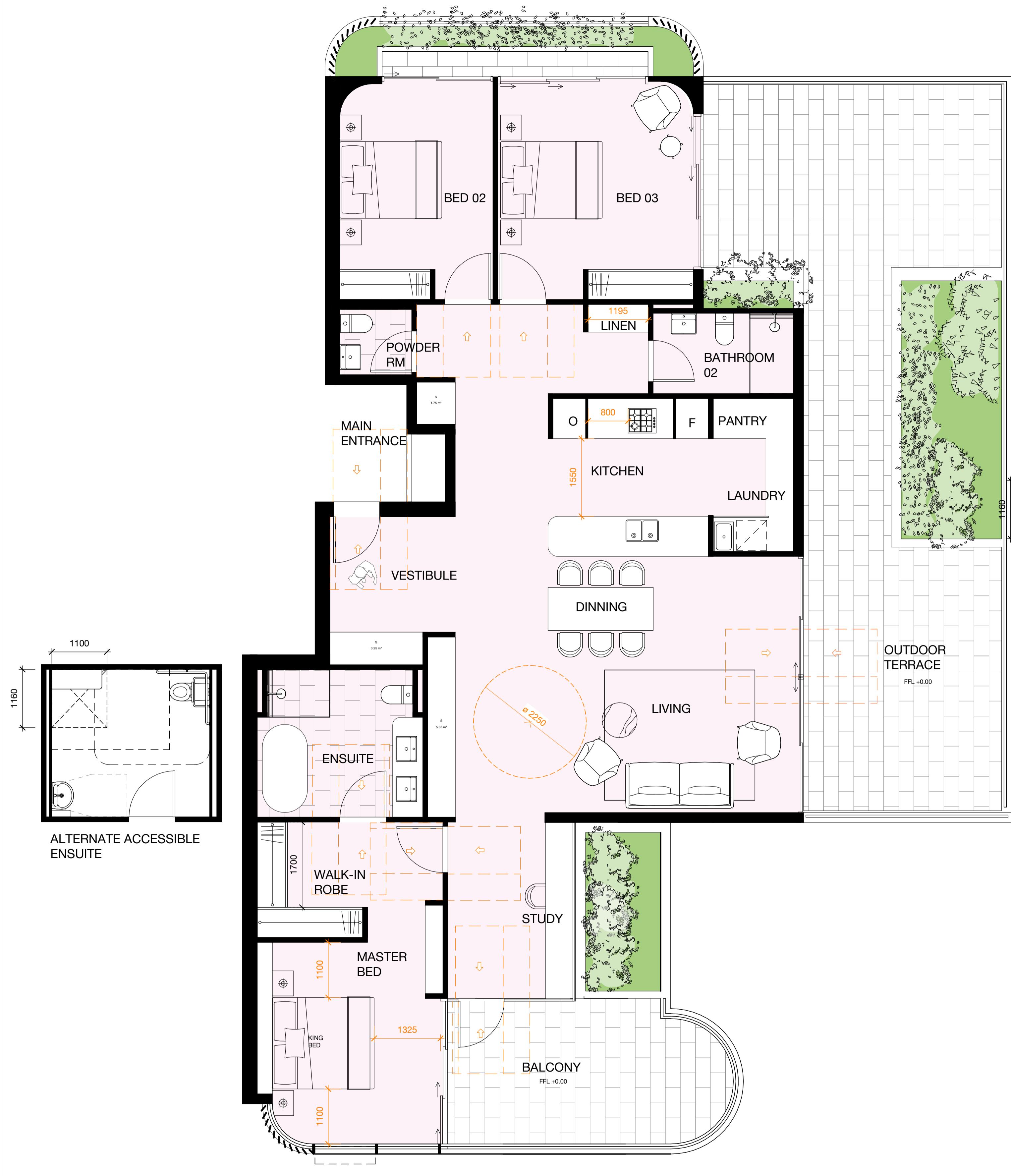
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A13 APARTMENT TYPE - 3B PENTHOUSE

Status	CONCEPT
Scale	As indicated @ A1
Drawn	SH Checked
Project No.	S12551
Pilot Date	8/10/2021 12:37:09 AM

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Drawing no. Revision

A13.004 A

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9 AM



10 AM



11 AM



12 PM



1 PM



2 PM



3 PM

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Legend

 PROPOSED DEVELOPMENT AT 671-683 OLD SOUTH HEAD ROAD VAUCLUSE

 SHADOW CAST BY PROPOSED DEVELOPMENT AT WINTER SOLSTICE JUNE 21ST

 APPROVED NEIGHBOURING DA

A	21.10.07 DEVELOPMENT APPLICATION	SH
1	21.10.01 ISSUE FOR INFORMATION	Initial
Rev	Date	Checked

OSHR AT VAUCLUSE HOLDINGS PTY LTD

VAUCLUSE SENIORS LIVING
671- 683 OSH RD VAUCLUSE

A21
SHADOW DIAGRAMS - PLAN

Status	CONCEPT	
Scale	1 : 100	@ A1
Drawn	Author	Checked
Project No.	S12551	
Plot Date	8/10/2021 12:37:18 AM	
BIM		

Drawing no. **A21.001** Revision **A**

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Bates Smart Architects Pty Ltd ABN 68 094 740 986



9 AM



10 AM



11 AM



12 PM



1 PM



2 PM



3 PM

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Legend

- PROPOSED DEVELOPMENT AT 671-683 OLD SOUTH HEAD ROAD VAUCLUSE
- SHADOW CAST BY PROPOSED DEVELOPMENT AT WINTER SOLSTICE JUNE 21ST
- APPROVED NEIGHBOURING DA

A	21.10.07 DEVELOPMENT APPLICATION	SH
1	21.10.01 ISSUE FOR INFORMATION	SH
Rev	Date	Description

			Initial	Checked
--	--	--	---------	---------

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VAUCLUSE SENIORS LIVING
671- 683 OSH RD VAUCLUSE

A21
SHADOW DIAGRAM -
PERSPECTIVE

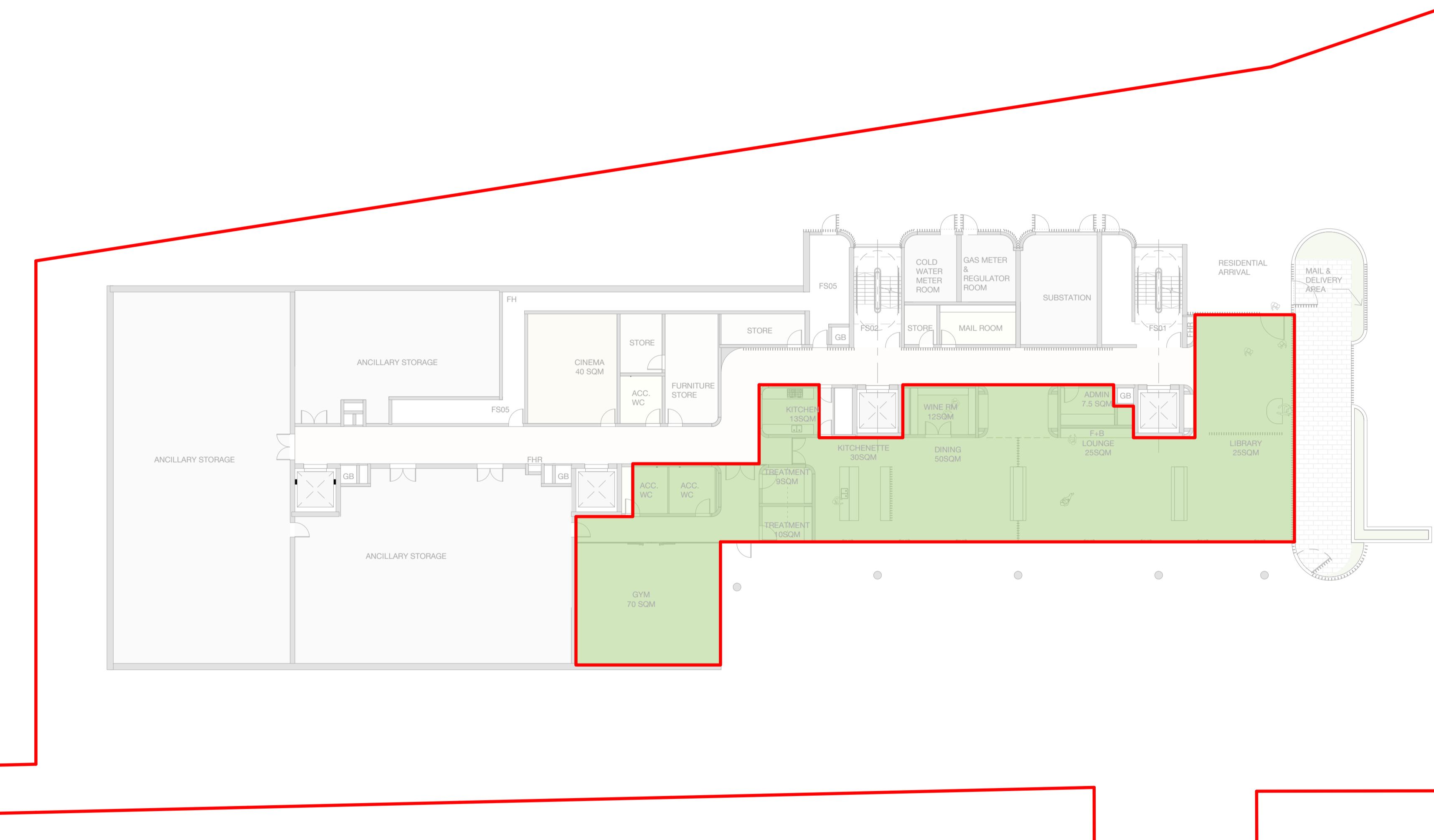
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Drawn	Author Checked
Project No.	S12551
Plot Date	8/10/2021 12:37:24 AM
BIM	
Drawing no.	Revision

A21.002 **A**

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VAUCLUSE SENIORS LIVING
671- 683 OSH RD VAUCLUSE

A22
AREA PLANS



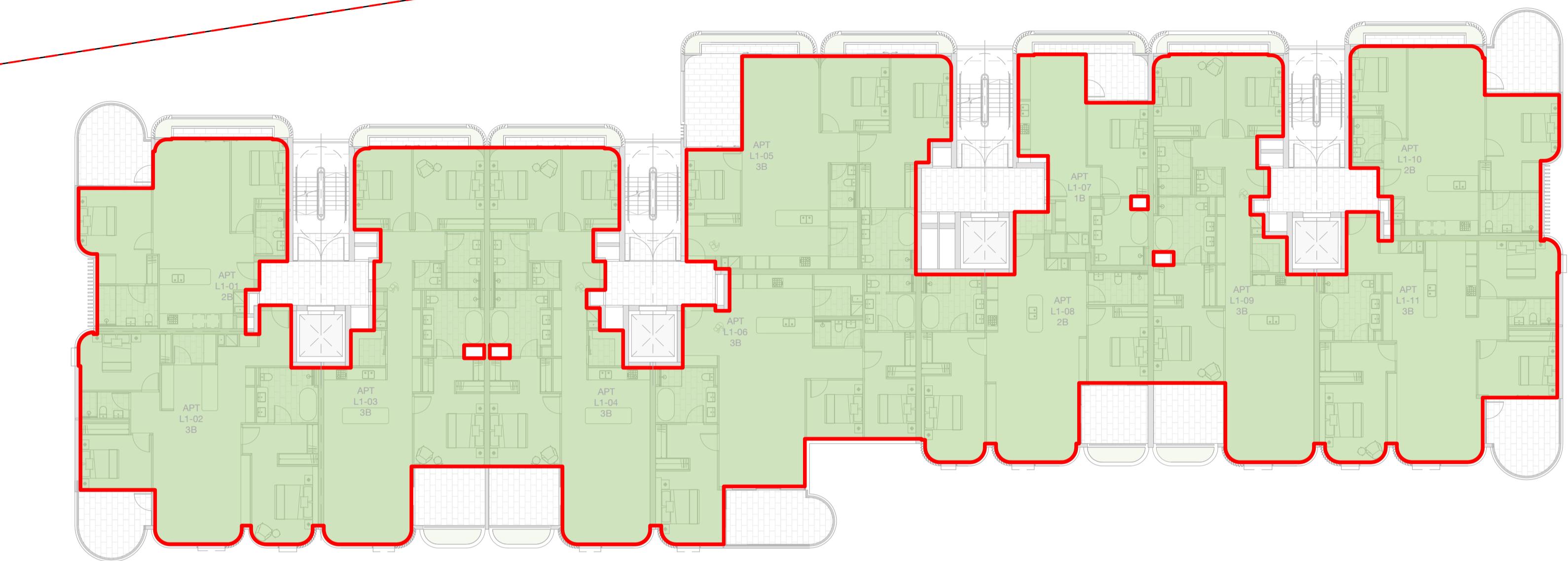
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Project No.	S12551
Plot Date	8/10/2021 12:37:35 AM
BIM	
Drawing no.	Revision

A22.001 **A**

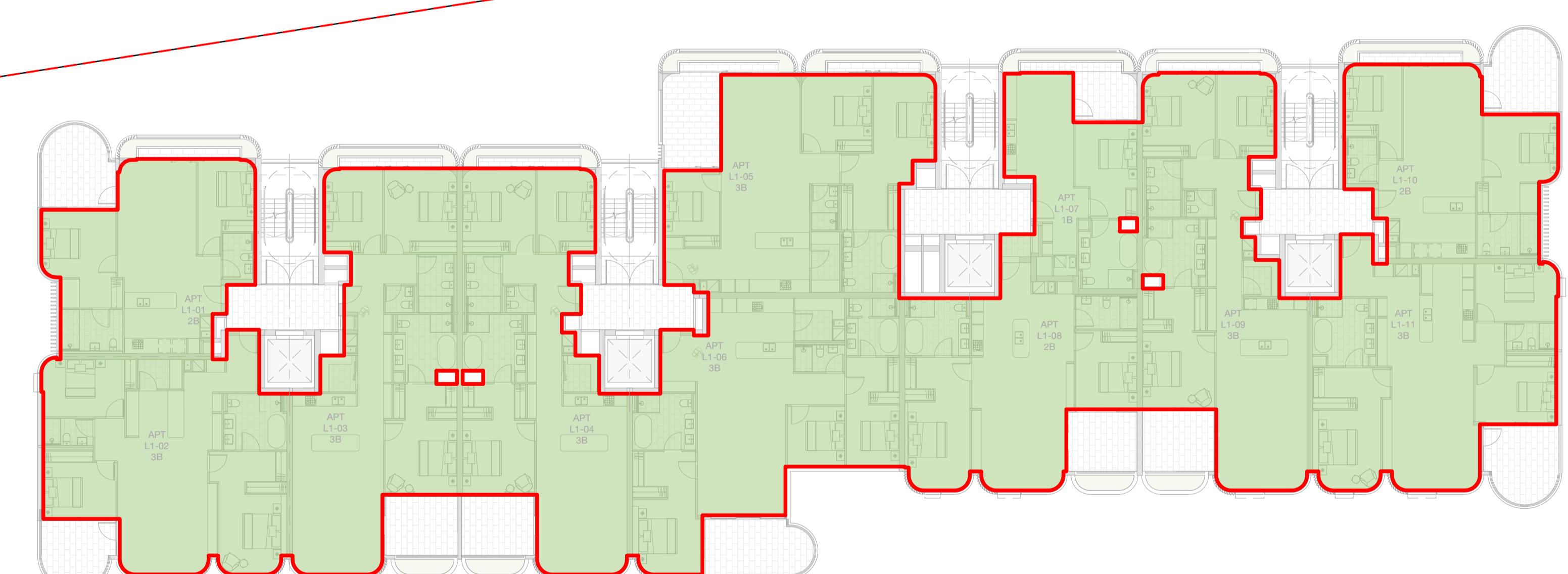
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GROUND FLOOR (UPPER)
RESIDENTIAL APARTMENTS
1,353 SQM



LEVEL 01
RESIDENTIAL APARTMENTS
1,353 SQM

A	21.10.07 DEVELOPMENT APPLICATION	SH
2	21.10.01 ISSUE FOR INFORMATION	SH
1	21.09.23 ISSUE FOR INFORMATION	SH
Rev	Date	Description
		Initial Checked

OSHR AT VAUCLUSE HOLDINGS PTY LTD

VAUCLUSE SENIORS LIVING
671- 683 OSH RD VAUCLUSE

A22
AREA PLANS



Status	CONCEPT
Scale	1 : 200 @ A1
Drawn	SH Checked
Project No.	S12551
Plot Date	8/10/2021 12:40:15 AM
BIM	
Drawing no.	Revision

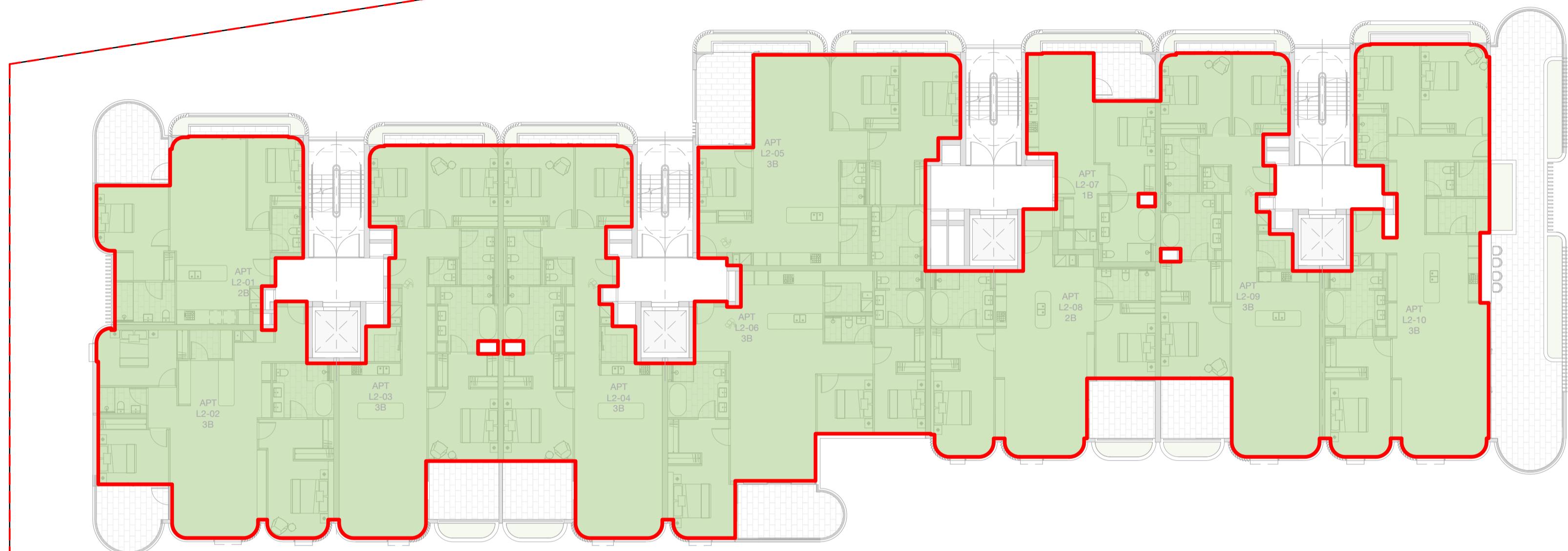
A22.002

A

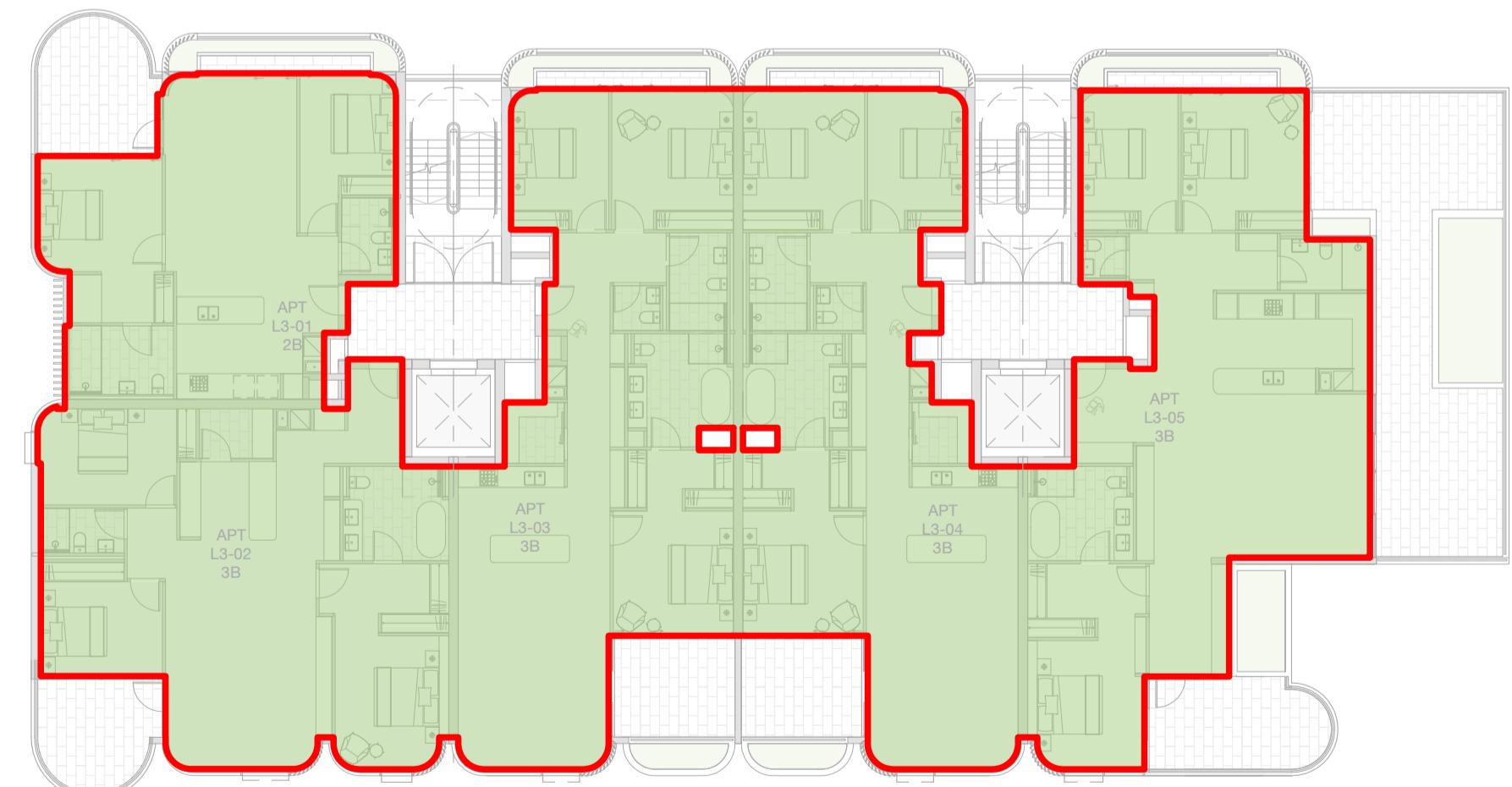
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LEVEL 02
RESIDENTIAL APARTMENTS
1,293 SQM



LEVEL 03
RESIDENTIAL APARTMENTS
673 SQM

A	21.10.07 DEVELOPMENT APPLICATION	SH
2	21.10.01 ISSUE FOR INFORMATION	SH
1	21.09.23 ISSUE FOR INFORMATION	SH
Rev	Date	Description
		Initial Checked

OSHR AT VAUCLUSE HOLDINGS PTY LTD

VAUCLUSE SENIORS LIVING
671- 683 OSH RD VAUCLUSE

A22
AREA PLANS



Status	CONCEPT
Scale	1 : 200 @ A1
Drawn	SH Checked
Project No.	S12551
Plot Date	8/10/2021 12:40:29 AM
BIM	
Drawing no.	Revision

A22.003 A

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1. BRICK
Balcony and walls



5. GLASS
Fixed, awning window and sliding doors



2. CONCRETE
Expressed floor slabs



5. METAL 01
All frames to glazing



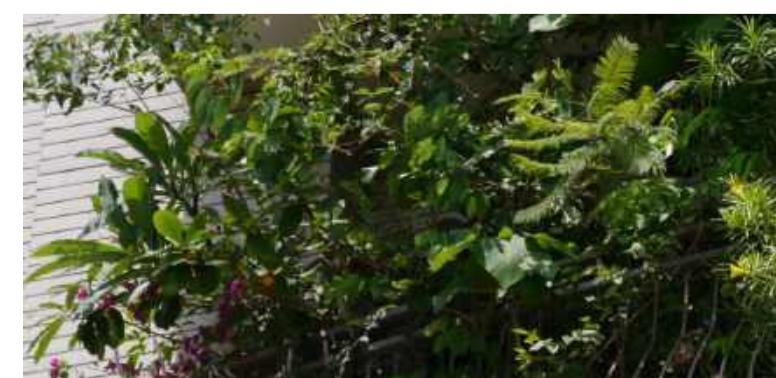
3. TERRACOTTA SCREEN
Screens for privacy, ventilation and shading



6. METAL 02
Balustrade handrail



4. GLASS BRICKS
Fire Stairs



7. PLANTING
Landscape to Juliette balcony and courtyard

Check all dimensions and site conditions prior to commencement of any work.
the purchase or ordering of any materials, fittings, plant, services or equipment
and the preparation of shop drawings and/or the fabrication of any components.
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OSHR AT VAUCLUSE HOLDINGS PTY LTD

VAUCLUSE SENIORS LIVING
671-683 OSH RD VAUCLUSE

A41 MATERIAL SCHEDULE

Status	CONCEPT
Scale	1 : 20 @ A1
Drawn	SH Checked
Project No.	S12551
Pilot Date	8/10/2021 12:40:41 AM
BIM	
Drawing no.	Revision

A41.001

A

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APPENDIX B
BOREHOLE LOGS INCLUDING SPT AND DCP TEST DATA (9 SHEETS)

Borehole Log Report

Geo Environmental Engineering Pty Ltd
82 Bridge Street
Lane Cove NSW 2066
T 02 9420 3361



Hole ID.

BH201

Hole Depth:

2,20 m

Sheet:

1 of 1

Project Name: **Geotechnical Investigation**

Project Number: G21071VAU

Location / Site: 671-683 Old South Head Road, Vaucluse NSW

Client: Blare Management

Drilling Company: **FICO Group**

Date Started: **19-AUG-21**

Ground Level: **RL66.1m** (approx)

Drill Method: **SFA**

Date Completed: **19-AUG-21**

Latitude: _____

Equipment: **Ute Mounted**

Longitude: -----

Moisture	Additional Comments
D Dry	
Dp Damp	
SM Slightly Moist	
M Moist	
VM Very Moist	
W Wet	
Sd Saturated	

Borehole Log Report

Geo Environmental Engineering Pty Ltd
82 Bridge Street
Lane Cove NSW 2066
T 02 9420 3361



Hole ID.

BH202

Hole Depth:

3.95 m

Sheet:

1 of 1

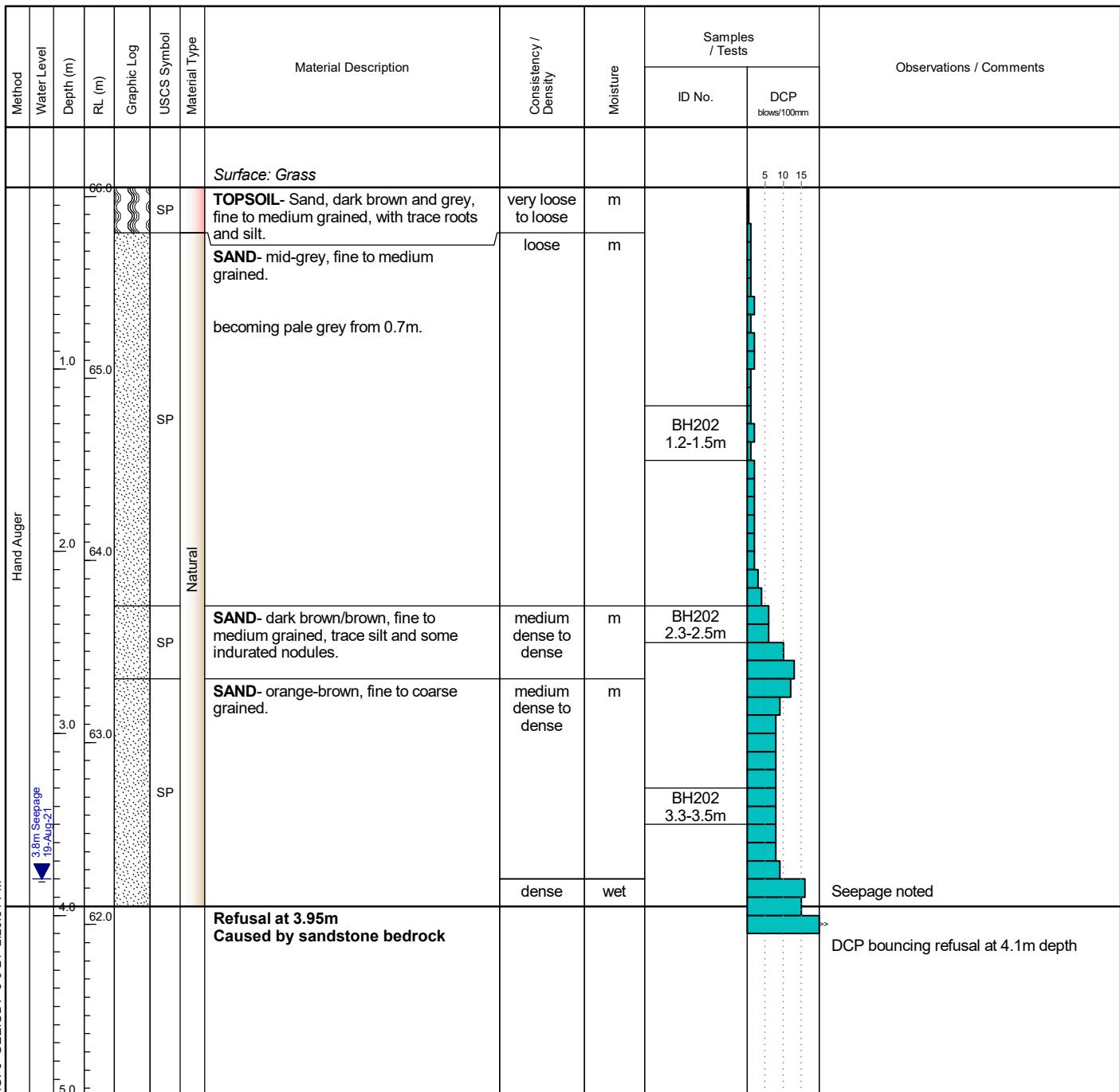
Project Name: **Geotechnical Investigation** Project Number: **G21071VAU**

Location / Site: **671-683 Old South Head Road, Vaucluse NSW** Client: **Blare Management**

Drilling Company: **Geo Environmental Engineering** Date Started: **19-AUG-21** Ground Level: **RL66.05m** (approx)

Drill Method: **Hand Auger** Date Completed: **19-AUG-21** Latitude: **-----**

Equipment: **Manual** Longitude: **-----**



Moisture		Additional Comments	
D	Dry		
Dp	Damp		
SM	Slightly Moist		
M	Moist		
VM	Very Moist		
W	Wet		
Sd	Saturated		

MATERIAL SYMBOL



FILL



CONCRETE



ASPHALT



TOPSOIL



ORGANICS



ESTUARINE MUD



CLAY



SAND



SILT



GRAVEL



Sandy CLAY



Clayey SAND



Clayey SILT



Clayey GRAVEL



Silty CLAY



Silty SAND



Sandy SILT



Sandy GRAVEL



Gravelly CLAY



Gravelly SAND



Gravelly SILT



Silty GRAVEL



CLAY & SAND



SAND & CLAY



SILT & CLAY



GRAVEL & CLAY



CLAY & SILT



SAND & SILT



SILT & SAND



GRAVEL & SAND



CLAY & GRAVEL



SAND & GRAVEL



SILT & GRAVEL



GRAVEL & SILT



Sandy Silty CLAY



Clayey Silty SAND



Sandy Clayey SILT



Sandy Clayey GRAVEL



Silty Sandy CLAY



Silty Clayey SAND



Clayey Sandy SILT



Clayey Sandy GRAVEL



Sandy Gravelly CLAY



Clayey Gravelly SAND



Sandy Gravelly SILT



Silty Clayey GRAVEL



Silty Gravelly CLAY



Silty Gravelly SAND



Clayey Gravelly SILT



Clayey Silty GRAVEL



Gravelly Silty CLAY



Gravelly Silty SAND



Gravelly Clayey SILT



Sandy Silty GRAVEL



Gravelly Sandy CLAY



Gravelly Clayey SAND



Gravelly Sandy SILT



Silty Sandy GRAVEL



SANDSTONE



SHALE



GRANITE



BASALT



SHALE / SANDSTONE



PORCELLANITE



GNEISS



SHALE / CLAYSTONE



MUDSTONE



CLAYSTONE



MUDSTONE / CLAYSTONE



SHALE / SILTSTONE



IRONSTONE

ATER LEVELS



Encountered Water



Standing Water

ABBREVIATIONS

PT

Pushtube

SFA

Solid Flight Auger

PWS

Percussion Window Sampler

HA

Hand Auger

HFA

Hollow Flight Auger

ELL RAPHICS



Cuttings



Bentonite



Screen



Gravel Pack



Grout



Cave-in

BOREHOLE REPORT

CLIENT: OSHR AT VAUCLUSE HOLDING PTY LTD

DATE: 28/06/2018

BORE No.: 1

PROJECT: 4 LEVEL RESIDENTIAL DEVELOPMENT

PROJECT No.: 2018-106

SHEET: 1 of 1

LOCATION: 671-679 OLD SOUTH HEAD ROAD,
VAUCLUSE

SURFACE LEVEL: RL 1 71.80m

Depth (m)	Description of Strata	Sampling		In Situ Testing	
		Type	Depth (m)	Type	Results
0.00	PRIMARY SOIL - strength/density, colour, grainsize/plasticity, moisture, soil type incl. secondary constituents, other remarks				
0.20	TOPSOIL: Dark brown				
0.70	FILL: Brown, fine to medium grained, sand fill				
1.00	SAND (SP): Loose, pale grey, fine to medium grained, moist sand (Superficial Soil)				
1.80	* became medium dense below 1.80m depth				
2.00					
2.60	Gravelly SAND (SW): Medium dense, brown, medium grained, sand, medium to coarse ground sub-rounded to rounded gravel, moist (Superficial Soil)	D	2.63-2.80		
2.80	Sandy CLAY (CL): Firm, orange, low plasticity, moist sandy clay (Residual Soil)	D	2.80-2.88		
3.00	* became very stiff to hard below 3.00m depth	D	3.30-3.40		
3.60	Sandstone (EW) Extremely low strength, orange brown, fine grained (Hawksbury Sandstone)				
3.80	HAND AUGER REFUSUAL @3.80m depth in interpreted hard sandy clay to extremely low strength sandstone				
4.00					

RIG: None

DRILLER: CL

LOGGED: JY

METHOD: Hand Auger

GROUND WATER OBSERVATIONS: no free ground water found

REMARKS:

CHECKED:

BOREHOLE REPORT

CLIENT: OSHR AT VAUCLUSE HOLDING
PTY LTD

DATE: 28/06/2018

BORE No.: 2

PROJECT: 4 LEVEL RESIDENTIAL
DEVELOPMENT

PROJECT No.: 2018-106

SHEET: 1 of 1

LOCATION: 671-679 OLD SOUTH HEAD ROAD,
VAUCLUSE

SURFACE LEVEL: RL 1 73.30m

Depth (m)	Description of Strata	Sampling		In Situ Testing	
		Type	Depth (m)	Type	Results
0.00	PRIMARY SOIL - strength/density, colour, grainsize/plasticity, moisture, soil type incl. secondary constituents, other remarks				
0.20	TOPSOIL: Dark brown				
0.70	FILL: Brown, fine to medium grained, sand fill				
1.00	SAND (SP): Loose, pale grey, fine to medium grained, moist sand (Superficial Soil)				
1.35	* became medium dense, orange brown and iron cemented between 1.35m to 1.75m depth				
1.75	* became orange yellow below 1.75m depth				
2.00					
2.85	* became dense below 2.85m depth				
3.00					
3.60	* became very dense below 3.60m depth				
4.00					
5.00					
5.20	HAND AUGER DISCONTINUED @5.20m depth				

RIG: None

DRILLER: CL

LOGGED: JY

METHOD: Hand Auger

GROUND WATER OBSERVATIONS: no free ground water found

REMARKS:

CHECKED:

BOREHOLE REPORT

CLIENT: OSHR AT VAUCLUSE HOLDING
PTY LTD

DATE: 28/06/2018

BORE No.: 3

PROJECT: 4 LEVEL RESIDENTIAL
DEVELOPMENT

PROJECT No.: 2018-106

SHEET: 1 of 1

LOCATION: 671-679 OLD SOUTH HEAD ROAD,
VAUCLUSE

SURFACE LEVEL: RL 1 73.00m

Depth (m)	Description of Strata	Sampling		In Situ Testing	
		Type	Depth (m)	Type	Results
0.00	PRIMARY SOIL - strength/density, colour, grainsize/plasticity, moisture, soil type incl. secondary constituents, other remarks				
0.20	TOPSOIL: Dark brown				
0.45	FILL: Brown, fine to medium grained, sand fill				
1.00	SAND (SP) : Very loose to loose, pale grey, fine to medium grained, moist sand (Superficial Soil) * became medium dense, brown orange and iron cemented below 1.00m depth				
1.20	HAND AUGER DISCONTINUED @1.20m depth in medium dense sand				
2.00					
3.00					
4.00					
5.00					

RIG: None

DRILLER: CL

LOGGED: JY

METHOD: Hand Auger

GROUND WATER OBSERVATIONS: no free ground water found

REMARKS:

CHECKED:

BOREHOLE REPORT

CLIENT: OSHR AT VAUCLUSE HOLDING PTY LTD

DATE: 28/06/2018

BORE No.: 4

PROJECT: 4 LEVEL RESIDENTIAL DEVELOPMENT

PROJECT No.: 2018-106

SHEET: 1 of 1

LOCATION: 671-679 OLD SOUTH HEAD ROAD, VAUCLUSE

SURFACE LEVEL: RL 1 71.00m

Depth (m)	Description of Strata PRIMARY SOIL - strength/density, colour, grainsize/plasticity, moisture, soil type incl. secondary constituents, other remarks	Sampling		In Situ Testing	
		Type	Depth (m)	Type	Results
0.00					
0.15	TILE overlaying BEDDING SAND FILL: Brown, fine to medium grained, sand fill				
0.95					
1.00	SAND (SP): Loose, pale grey, fine to medium grained, moist sand (Superficial Soil)				
1.40	* became medium dense, red brown and iron cemented below 1.40m				
1.65	* became very dense between 1.65m to 1.95m depth				
1.95	* became medium dense, orange yellow below 1.95m depth				
2.00					
3.00					
4.00	* became dense below 4.05m depth				
5.00	HAND AUGER DISCONTINUED @5.00m depth				

RIG: None

DRILLER: CL

LOGGED: JY

METHOD: Hand Auger

GROUND WATER OBSERVATIONS: no free ground water found

REMARKS:

CHECKED:

BOREHOLE REPORT

CLIENT: OSHR AT VAUCLUSE HOLDING PTY LTD

DATE: 28/06/2018

BORE No.: 5

PROJECT: 4 LEVEL RESIDENTIAL DEVELOPMENT

PROJECT No.: 2018-106

SHEET: 1 of 1

LOCATION: 671-679 OLD SOUTH HEAD ROAD, VAUCLUSE

SURFACE LEVEL: RL 1 71.00m

Depth (m)	Description of Strata PRIMARY SOIL - strength/density, colour, grainsize/plasticity, moisture, soil type incl. secondary constituents, other remarks	Sampling		In Situ Testing	
		Type	Depth (m)	Type	Results
0.00	FILL: Brown, fine to medium grained, sand fill				
0.55	SAND (SP): Very loose, pale grey, fine to medium grained, moist sand (Superficial Soil)				
1.00	1.20 * became loose below 1.20m depth				
1.75	1.75 * became medium dense, red brown and iron cemented below 1.75m depth				
2.00	2.00 * became dense to very dense between 1.95m to 2.25m depth				
2.35	2.35 * became medium dense and orange yellow below 2.35m depth				
3.00					
3.45	3.45 * became dense below 3.45m depth				
3.75	3.75 * became very dense below 3.75m depth				
4.00					
5.00					
5.80	5.80 HAND AUGER DISCONTINUED @5.80m depth				
6.00					

RIG: None

DRILLER: CL

LOGGED: JY

METHOD: Hand Auger

GROUND WATER OBSERVATIONS: no free ground water found

REMARKS: -----

CHECKED: -----

DYNAMIC PENETROMETER TEST RESULTS SHEET

CLIENT: OSHR AT VAUCLUSE HOLDING **DATE:** 28/06/2018
PROJECT: 4 LEVEL RESIDENTIAL DEVELOPMENT **PROJECT No.:** 2018-106
LOCATION: 671-679 OLD SOUTH HEAD ROAD,
VAUCLUSE **SHEET:** 1 of 1

Depth (m)	Test Location								
	DCP1	DCP1a	DCP2	DCP2a	DCP3	DCP4	DCP4a	DCP5	DCP5a
0.00 - 0.15	1	--	1	--	2	13	--	--	--
0.15 - 0.30	1	--	2	--	1	2	--	--	--
0.30 - 0.45	1	--	2	--	0	3	--	--	--
0.45 - 0.60	1	--	2	--	0	3	--	1	--
0.60 - 0.75	1	--	2	--	2	2	--	1	--
0.75 - 0.90	2	--	2	--	2	2	--	1	--
0.90 - 1.05	2	--	2	--	4	2	--	1	--
1.05 - 1.20	2	--	2	--	6	2	--	1	--
1.20 - 1.35	2	--	3	--	5	3	--	2	--
1.35 - 1.50	2	--	5	--	3	3	--	2	--
1.50 - 1.65	3	--	4	--	4	3	--	2	--
1.65 - 1.80	3	--	4	--	4	16	--	5	--
1.80 - 1.95	4	--	3	--	5	12	--	6	--
1.95 - 2.10	4	--	4	--	6	7	--	14	--
2.10 - 2.25	5	--	4	--	7	6	--	17	--
2.25 - 2.40	6	--	5	--	8	7	--	9	--
2.40 - 2.55		--		--			--		--
2.55 - 2.70		--		--			--		--
2.70 - 2.85		8		7			5		--
2.85 - 3.00		3		14			5		--
3.00 - 3.15		7		12			4		--
3.15 - 3.30		18		13			3		4
3.30 - 3.45		29		12			4		10
3.45 - 3.60		40		14			3		14
3.60 - 3.75				19			3		14
3.75 - 3.90				19			6		17
3.90 - 4.05				22			9		18
4.05 - 4.20							11		21
4.20 - 4.35									

TEST METHOD: AS 1289. F3.2, CONE PENETROMETER -- DCP2a, 4a
AS 1289. F3.3, PERTH SAND PENETROMETER -- DCP1, 2, 3, 4, 5, 1a, 5a

REMARKS: (B) Test hammer bouncing upon refusal on solid object
-- No test undertaken at this level due to prior excavation of soils

Geotechnical investigation Report
671 - 683 Old South Head Road, Vaucluse Bay NSW



APPENDIX C

LABORATORY REPORT (7 SHEETS)

Environment Testing

Geo-Environmental Engineering Pty Ltd
 82 Bridge St
 Lane Cove
 NSW 2066



NATA Accredited
 Accreditation Number 1261
 Site Number 18217

Accredited for compliance with ISO/IEC 17025 – Testing
 NATA is a signatory to the ILAC Mutual Recognition
 Arrangement for the mutual recognition of the
 equivalence of testing, medical testing, calibration,
 inspection, proficiency testing scheme providers and
 reference materials producers reports and certificates.

Attention: ALL INVOICES Stephen McCormack

Report 818375-S
 Project name VAUCLUSE
 Received Date Aug 19, 2021

Client Sample ID			BH201/1-1.45	BH201/1.6-1.8	BH202/1.2-1.5	BH202/2.3-2.5
Sample Matrix			Soil	Soil	Soil	Soil
Eurofins Sample No.			S21-Au36223	S21-Au36224	S21-Au36225	S21-Au36226
Date Sampled			Aug 19, 2021	Aug 19, 2021	Aug 19, 2021	Aug 19, 2021
Test/Reference	LOR	Unit				
Chloride	10	mg/kg	< 10	< 10	< 10	10
Conductivity (1:5 aqueous extract at 25°C as rec.)	10	uS/cm	18	16	16	22
pH (1:5 Aqueous extract at 25°C as rec.)	0.1	pH Units	7.0	6.9	6.3	6.2
Resistivity*	0.5	ohm.m	540	620	620	450
Sulphate (as SO4)	10	mg/kg	< 10	< 10	< 10	13
% Moisture	1	%	6.9	7.8	1.8	5.4

Client Sample ID			BH202/3.3-3.5
Sample Matrix			Soil
Eurofins Sample No.			S21-Au36227
Date Sampled			Aug 19, 2021
Test/Reference	LOR	Unit	
Chloride	10	mg/kg	< 10
Conductivity (1:5 aqueous extract at 25°C as rec.)	10	uS/cm	10
pH (1:5 Aqueous extract at 25°C as rec.)	0.1	pH Units	6.6
Resistivity*	0.5	ohm.m	970
Sulphate (as SO4)	10	mg/kg	< 10
% Moisture	1	%	6.6

Sample History

Where samples are submitted/analysed over several days, the last date of extraction is reported.

If the date and time of sampling are not provided, the Laboratory will not be responsible for compromised results should testing be performed outside the recommended holding time.

Description	Testing Site	Extracted	Holding Time
Chloride	Sydney	Aug 23, 2021	28 Days
- Method: LTM-INO-4090 Chloride by Discrete Analyser			
Conductivity (1:5 aqueous extract at 25°C as rec.)	Sydney	Aug 23, 2021	7 Days
- Method: LTM-INO-4030 Conductivity			
pH (1:5 Aqueous extract at 25°C as rec.)	Sydney	Aug 23, 2021	7 Days
- Method: LTM-GEN-7090 pH in soil by ISE			
Sulphate (as SO ₄)	Sydney	Aug 23, 2021	28 Days
- Method: E045 Anions by Ion Chromatography			
% Moisture	Sydney	Aug 19, 2021	14 Days
- Method: LTM-GEN-7080 Moisture			

**Australia****Environment Testing**

ABN: 50 005 085 521 web: www.eurofins.com.au email: EnviroSales@eurofins.com

Company Name: Geo-Environmental Engineering P/L
Address: 82 Bridge St.
 Lane Cove
 NSW 2066

Project Name: VAUCLUSE

Order No.:
Report #:
Phone:
Fax:

818375
 02 9592 0218
 02 9519 9140

Moisture Set

Aggressivity Soil Set

Sample Detail**Melbourne Laboratory - NATA Site # 1254****Sydney Laboratory - NATA Site # 18217****Brisbane Laboratory - NATA Site # 20794****Perth Laboratory - NATA Site # 23736****Mayfield Laboratory - NATA Site # 25079****External Laboratory**

No	Sample ID	Sample Date	Sampling Time	Matrix	LAB ID
1	BH201/1.1.45	Aug 19, 2021		Soil	S21-Au36223
2	BH201/1.6-1.8	Aug 19, 2021		Soil	S21-Au36224
3	BH202/1.2-1.5	Aug 19, 2021		Soil	S21-Au36225
4	BH202/2.3-2.5	Aug 19, 2021		Soil	S21-Au36226
5	BH202/3.3-3.5	Aug 19, 2021		Soil	S21-Au36227

Test Counts

5

5

5

5

5

New Zealand

Melbourne
 6 Monterey Road
 Dandenong South VIC 3175
 Phone :+61 3 8564 5000
 NATA # 1261 Site # 1254

Sydney
 Unit F3, Building F
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 Lane Cove West NSW 2066
 Phone :+61 7 3902 4600
 NATA # 1261 Site # 20794
 NATA # 1261 Site # 18217

Brisbane
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 Murarrie QLD 4172
 Phone :+61 7 3902 4600
 NATA # 1261 Site # 20794
 NATA # 1261 Site # 18217

Auckland
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 IANZ # 1327

Newcastle
 4/52 Industrial Drive
 Mayfield East NSW 2304
 PO Box 60 Wichtham 2293
 Phone :+61 2 4968 8448
 NATA # 1261 Site # 25079

Received: Aug 19, 2021 3:05 PM**Due:** Aug 26, 2021**Priority:** 5 Day**Contact Name:** ALL INVOICES Stephen**Eurofins Analytical Services Manager : Andrew Black**

Internal Quality Control Review and Glossary

General

1. Laboratory QC results for Method Blanks, Duplicates, Matrix Spikes, and Laboratory Control Samples follows guidelines delineated in the National Environment Protection (Assessment of Site Contamination) Measure 1999, as amended May 2013 and are included in this QC report where applicable. Additional QC data may be available on request.
2. All soil/sediment/solid results are reported on a dry basis, unless otherwise stated.
3. All biota/food results are reported on a wet weight basis on the edible portion, unless otherwise stated.
4. Actual LORs are matrix dependant. Quoted LORs may be raised where sample extracts are diluted due to interferences.
5. Results are uncorrected for matrix spikes or surrogate recoveries except for PFAS compounds.
6. SVOC analysis on waters are performed on homogenised, unfiltered samples, unless noted otherwise.
7. Samples were analysed on an 'as received' basis.
8. Information identified on this report with blue colour, indicates data provided by customer, that may have an impact on the results.
9. This report replaces any interim results previously issued.

Holding Times

Please refer to 'Sample Preservation and Container Guide' for holding times (QS3001).

For samples received on the last day of holding time, notification of testing requirements should have been received at least 6 hours prior to sample receipt deadlines as stated on the SRA.

If the Laboratory did not receive the information in the required timeframe, and regardless of any other integrity issues, suitably qualified results may still be reported.

Holding times apply from the date of sampling, therefore compliance to these may be outside the laboratory's control.

For VOCs containing vinyl chloride, styrene and 2-chloroethyl vinyl ether the holding time is 7 days however for all other VOCs such as BTEX or C6-10 TRH then the holding time is 14 days.

****NOTE:** pH duplicates are reported as a range NOT as RPD

Units

mg/kg: milligrams per kilogram

mg/L: milligrams per litre

ug/L: micrograms per litre

ppm: Parts per million

ppb: Parts per billion

%: Percentage

org/100mL: Organisms per 100 millilitres

NTU: Nephelometric Turbidity Units

MPN/100mL: Most Probable Number of organisms per 100 millilitres

Terms

Dry	Where a moisture has been determined on a solid sample the result is expressed on a dry basis.
LOR	Limit of Reporting.
SPIKE	Addition of the analyte to the sample and reported as percentage recovery.
RPD	Relative Percent Difference between two Duplicate pieces of analysis.
LCS	Laboratory Control Sample - reported as percent recovery.
CRM	Certified Reference Material - reported as percent recovery.
Method Blank	In the case of solid samples these are performed on laboratory certified clean sands and in the case of water samples these are performed on de-ionised water.
Surr - Surrogate	The addition of a like compound to the analyte target and reported as percentage recovery.
Duplicate	A second piece of analysis from the same sample and reported in the same units as the result to show comparison.
USEPA	United States Environmental Protection Agency
APHA	American Public Health Association
TCLP	Toxicity Characteristic Leaching Procedure
COC	Chain of Custody
SRA	Sample Receipt Advice
QSM	US Department of Defense Quality Systems Manual Version 5.3
CP	Client Parent - QC was performed on samples pertaining to this report
NCP	Non-Client Parent - QC performed on samples not pertaining to this report, QC is representative of the sequence or batch that client samples were analysed within.
TEQ	Toxic Equivalency Quotient

QC - Acceptance Criteria

RPD Duplicates: Global RPD Duplicates Acceptance Criteria is 30% however the following acceptance guidelines are equally applicable:

Results <10 times the LOR : No Limit

Results between 10-20 times the LOR : RPD must lie between 0-50%

Results >20 times the LOR : RPD must lie between 0-30%

Surrogate Recoveries: Recoveries must lie between 20-130% Phenols & 50-150% PFASs

PFAS field samples that contain surrogate recoveries in excess of the QC limit designated in QSM 5.3 where no positive PFAS results have been reported have been reviewed and no data was affected.

WA DWER (n=10): PFBA, PFPeA, PFHxA, PFHpA, PFOA, PFBS, PFHxS, PFOS, 6:2 FTSA, 8:2 FTSA

QC Data General Comments

1. Where a result is reported as a less than (<), higher than the nominated LOR, this is due to either matrix interference, extract dilution required due to interferences or contaminant levels within the sample, high moisture content or insufficient sample provided.
2. Duplicate data shown within this report that states the word "BATCH" is a Batch Duplicate from outside of your sample batch, but within the laboratory sample batch at a 1:10 ratio. The Parent and Duplicate data shown is not data from your samples.
3. Organochlorine Pesticide analysis - where reporting LCS data, Toxaphene & Chlordane are not added to the LCS.
4. Organochlorine Pesticide analysis - where reporting Spike data, Toxaphene is not added to the Spike.
5. Total Recoverable Hydrocarbons - where reporting Spike & LCS data, a single spike of commercial Hydrocarbon products in the range of C12-C30 is added and it's Total Recovery is reported in the C10-C14 cell of the Report.
6. pH and Free Chlorine analysed in the laboratory - Analysis on this test must begin within 30 minutes of sampling. Therefore laboratory analysis is unlikely to be completed within holding time. Analysis will begin as soon as possible after sample receipt.
7. Recovery Data (Spikes & Surrogates) - where chromatographic interference does not allow the determination of Recovery the term "INT" appears against that analyte.
8. Polychlorinated Biphenyls are spiked only using Aroclor 1260 in Matrix Spikes and LCS.
9. For Matrix Spikes and LCS results a dash "-" in the report means that the specific analyte was not added to the QC sample.
10. Duplicate RPDs are calculated from raw analytical data thus it is possible to have two sets of data.

Quality Control Results

Test		Units	Result 1			Acceptance Limits	Pass Limits	Qualifying Code
Method Blank								
Chloride		mg/kg	< 10			10	Pass	
Conductivity (1:5 aqueous extract at 25°C as rec.)		uS/cm	< 10			10	Pass	
Sulphate (as SO4)		mg/kg	< 10			10	Pass	
LCS - % Recovery								
Chloride		%	103			70-130	Pass	
Conductivity (1:5 aqueous extract at 25°C as rec.)		%	80			70-130	Pass	
Resistivity*		%	80			70-130	Pass	
Sulphate (as SO4)		%	103			70-130	Pass	
Test	Lab Sample ID	QA Source	Units	Result 1		Acceptance Limits	Pass Limits	Qualifying Code
Spike - % Recovery								
				Result 1				
Chloride	S21-Au36225	CP	%	97			70-130	Pass
Sulphate (as SO4)	S21-Au36225	CP	%	98			70-130	Pass
Test	Lab Sample ID	QA Source	Units	Result 1		Acceptance Limits	Pass Limits	Qualifying Code
Duplicate								
				Result 1	Result 2	RPD		
% Moisture	S21-Au35685	NCP	%	11	13	20	30%	Pass
Duplicate								
				Result 1	Result 2	RPD		
Conductivity (1:5 aqueous extract at 25°C as rec.)	S21-Au36224	CP	uS/cm	16	13	26	30%	Pass
pH (1:5 Aqueous extract at 25°C as rec.)	S21-Au36224	CP	pH Units	6.9	6.9	<1	30%	Pass
Resistivity*	S21-Au36224	CP	ohm.m	620	800	26	30%	Pass
Duplicate								
				Result 1	Result 2	RPD		
Chloride	S21-Au36225	CP	mg/kg	< 10	< 10	<1	30%	Pass
Sulphate (as SO4)	S21-Au36225	CP	mg/kg	< 10	< 10	<1	30%	Pass

Comments

Sample Integrity

Custody Seals Intact (if used)	N/A
Attempt to Chill was evident	No
Sample correctly preserved	Yes
Appropriate sample containers have been used	Yes
Sample containers for volatile analysis received with minimal headspace	Yes
Samples received within HoldingTime	Yes
Some samples have been subcontracted	No

Authorised by:



Glenn Jackson
General Manager

Final Report – this report replaces any previously issued Report

- Indicates Not Requested

* Indicates NATA accredited

Measurement uncertainty of test data is available on request or please [click here](#).

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CHAIN OF CUSTODY RECORD

Sydney Laboratory
Unit F3 Buff 16 Mars Road Lane Cove West NSW 2066
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EnviroSampleNSW@eurofins.com

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07 3902 4600 EnviroSampleWA@eurofins.com

Perth Laboratory
Unit 2/91 Leach Highway Kewdale WA 6105
08 9251 9600 EnviroSampleWA@eurofins.com

Melbourne Laboratory
6 Monterey Road Dandenong South VIC 3175
03 8564 5000 EnviroSampleVIC@eurofins.com

Company	GEO-ENVIRONMENTAL																																																															
Address	82 BRIDGE ST LANE COVE																																																															
Contact Name	S. McCormack																																																															
Phone No	0431480980																																																															
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Submission of samples to the laboratory will be deemed as acceptance of Eurofins' Environment Testing Standard Terms and Conditions unless agreed otherwise. A copy is available on request.